

Towards a better understanding of meteoric
 ^{10}Be and ^9Be dynamics in river sediments

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MS Thesis Defense
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main objectives

Part 1. ^{10}Be and ^9Be dynamics in fluvial systems

gain understanding of the meteoric ^{10}Be proxy system by analyzing the composition of sediment grain coatings

assess the relative influences of remobilization processes, spatial heterogeneity of ^{10}Be and ^9Be inputs, and denudation rates on meteoric $^{10}\text{Be}/^9\text{Be}$ ratios of fluvial sediments

Part 2. meteoric $^{10}\text{Be}/^9\text{Be}$ -denudation rates

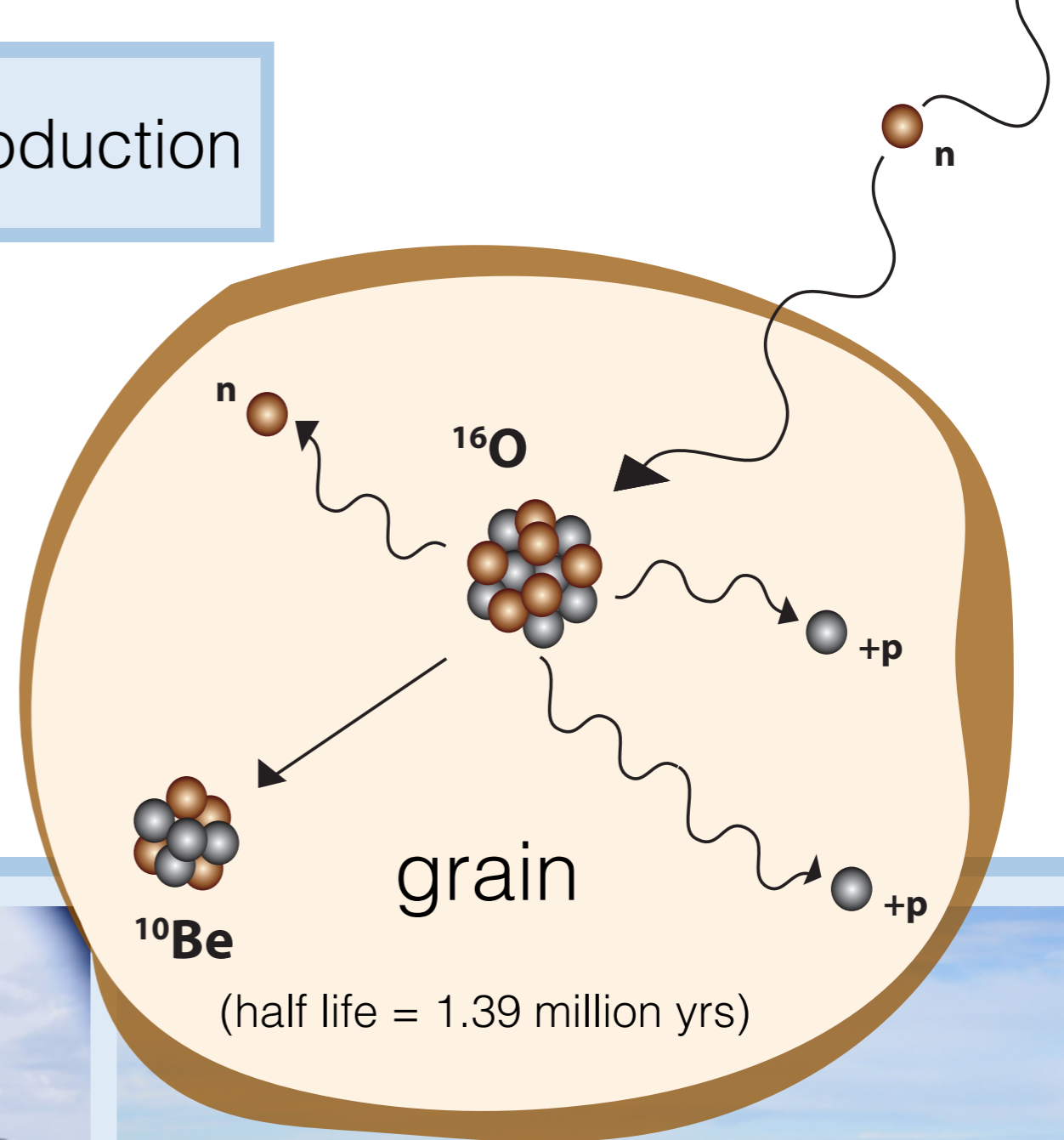
Compare meteoric $^{10}\text{Be}/^9\text{Be}$ denudation rates to known denudation rates (in situ based)

Outline

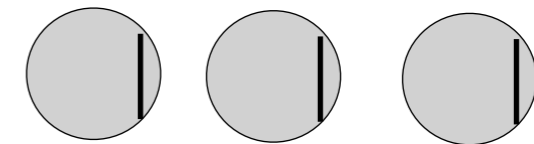
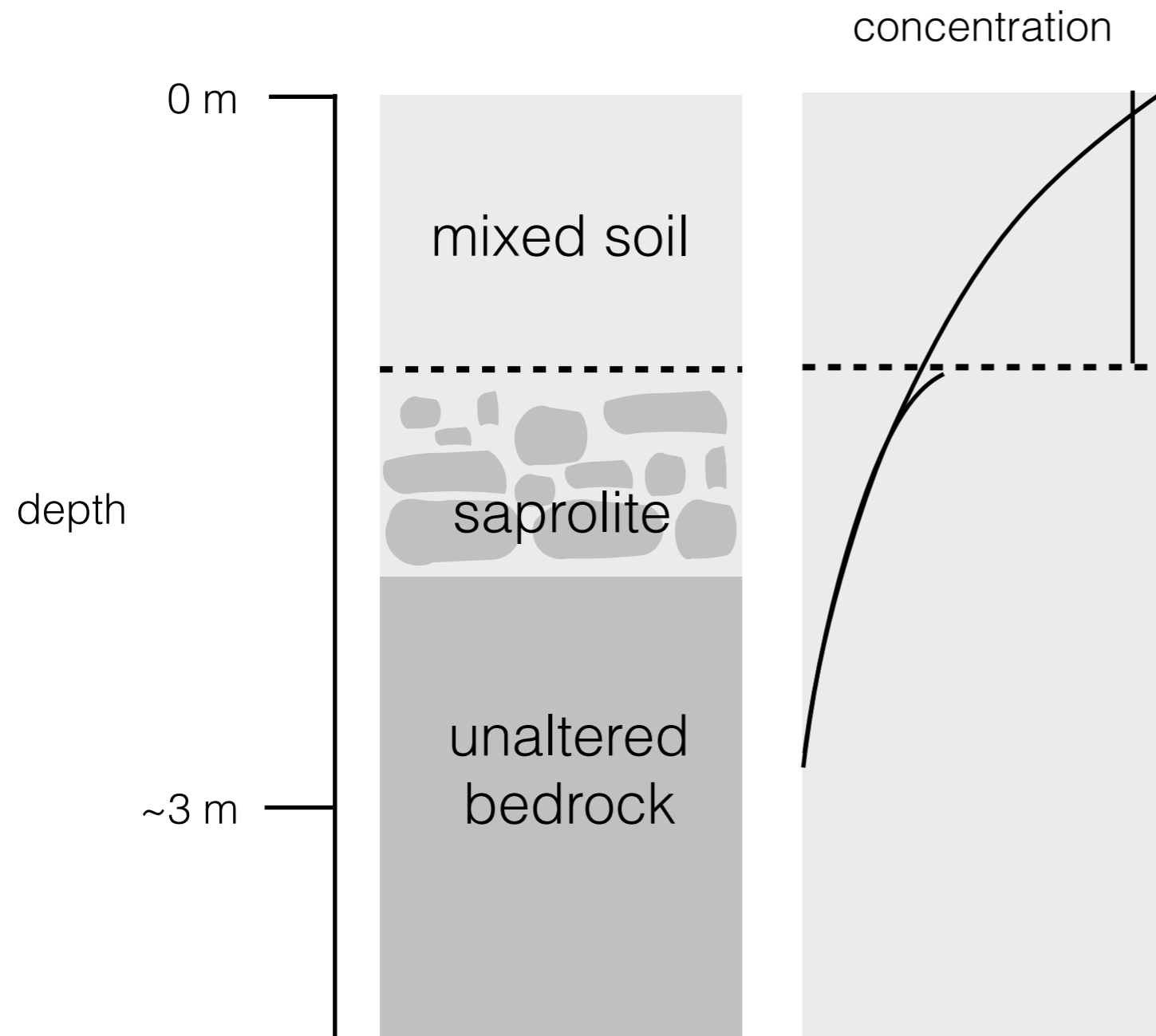
- Background
 - *in situ* ^{10}Be
 - *meteoric* ^{10}Be
 - *native* ^9Be
 - *meteoric* $^{10}\text{Be}/^9\text{Be}$ denudation rates
- Motivation and goals
- Methods
- Results
- Discussion
- Conclusions

background, part 1. *in situ* ^{10}Be production

- ^{10}Be trapped in mineral grains
- Production determined by well-understood physics



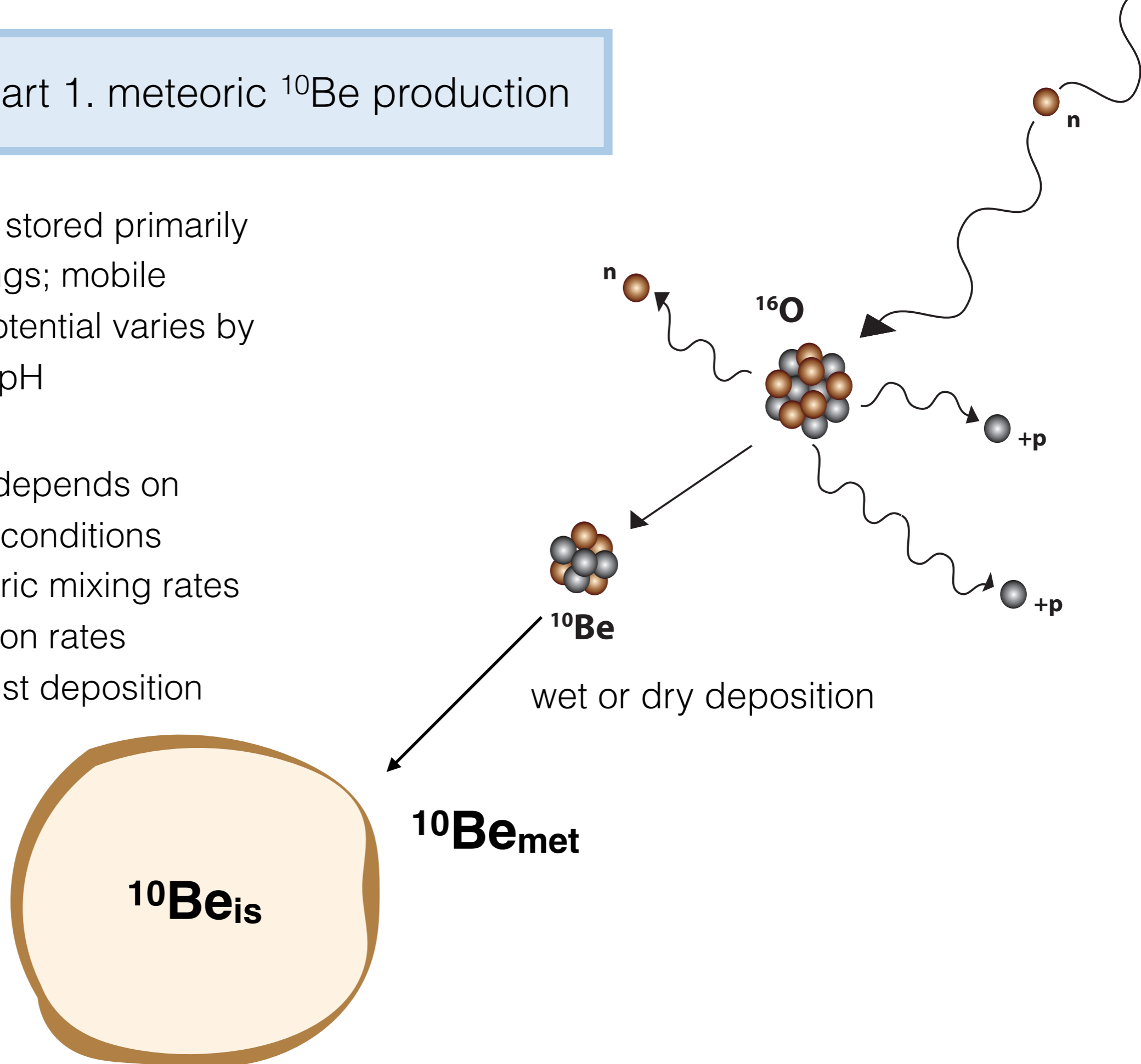
background, part 1. *in situ* ^{10}Be denudation rates



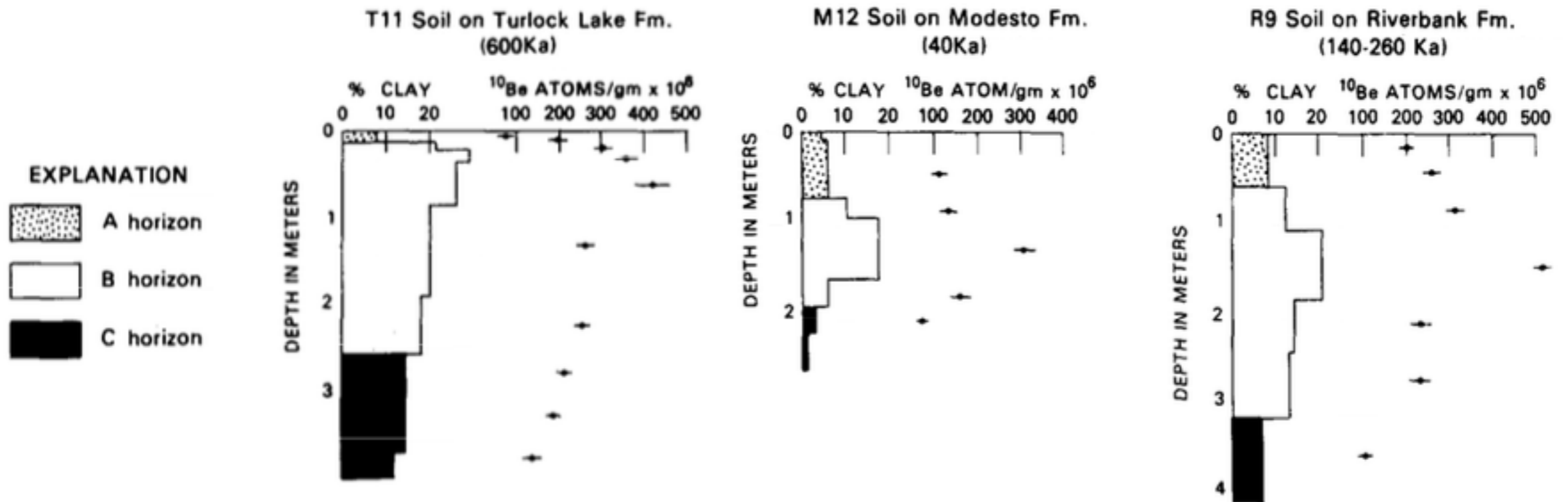
- slower denudation rates \rightarrow more *in situ* ^{10}Be in grains
- need to have sand-size grains or greater and quartz lithology

background, part 1. meteoric ^{10}Be production

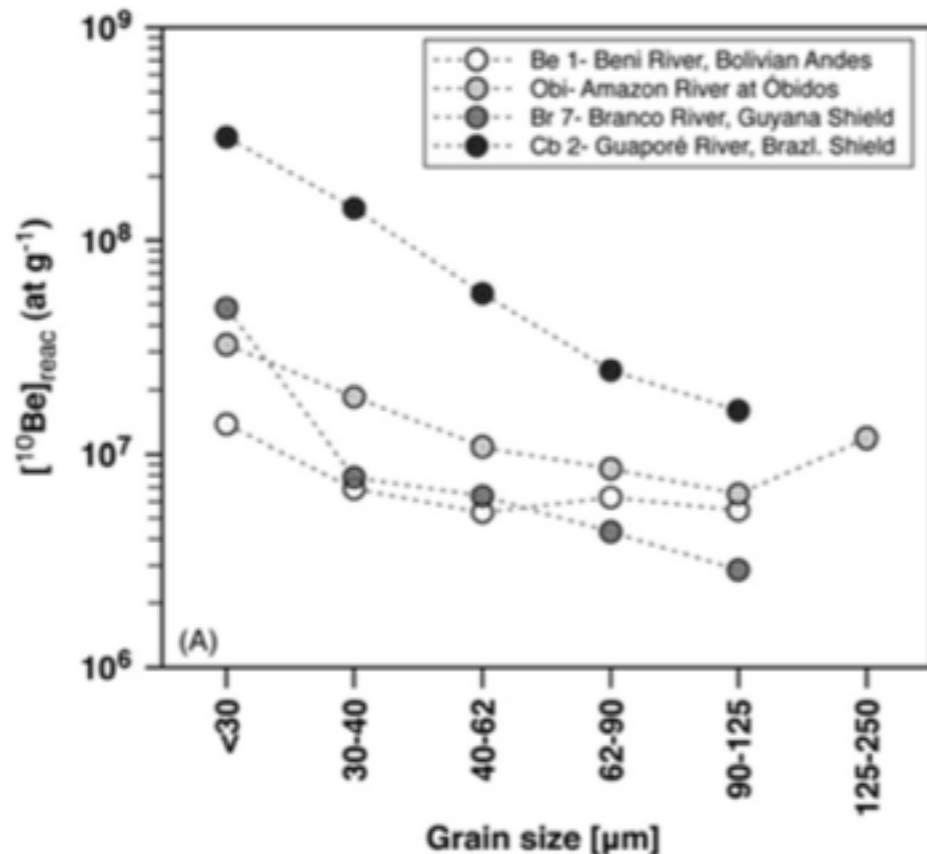
- meteoric ^{10}Be stored primarily in grain coatings; mobile
 - sorption potential varies by substrate, pH
- Delivery rate depends on
 - irradiation conditions
 - atmospheric mixing rates
 - precipitation rates
 - rates of dust deposition



background, part 1. meteoric ^{10}Be dynamics



river terraces, California. *Geochimica et Cosmochimica Acta*.



- correlates to % clay in soil profile
 - mineralogy (Cation Exchange Capacity)
 - grain size
- meteoric ^{10}Be abundance can be difficult to interpret

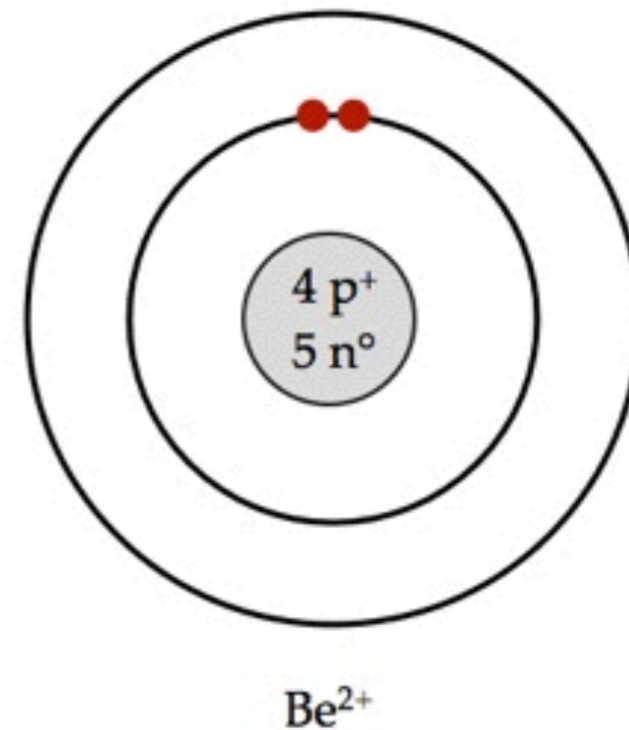
background, part 1. native ^9Be

~100% of natural abundance

beryl $\text{Be}_3\text{Al}_2(\text{SiO}_3)_6$



Be^{2+} ion

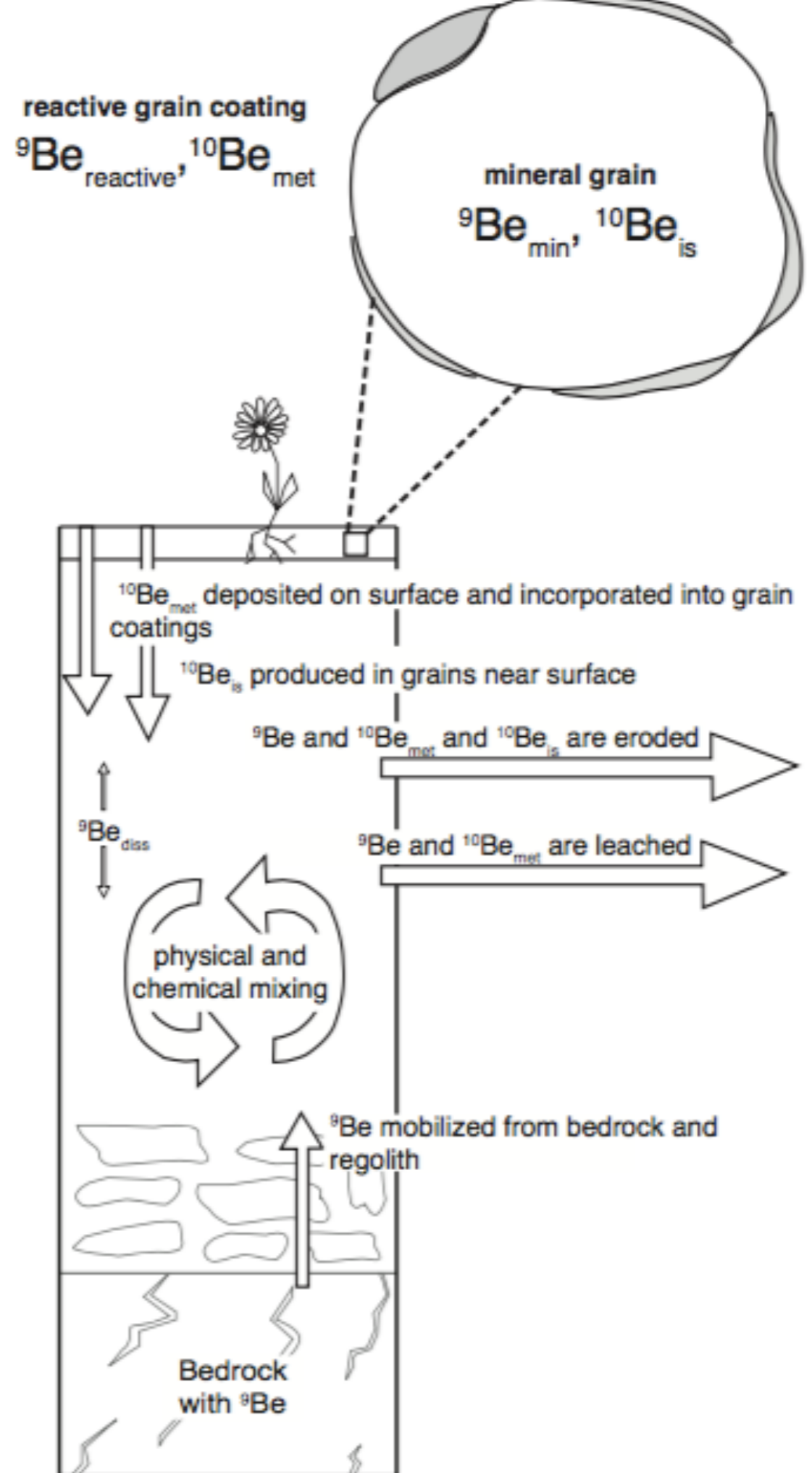
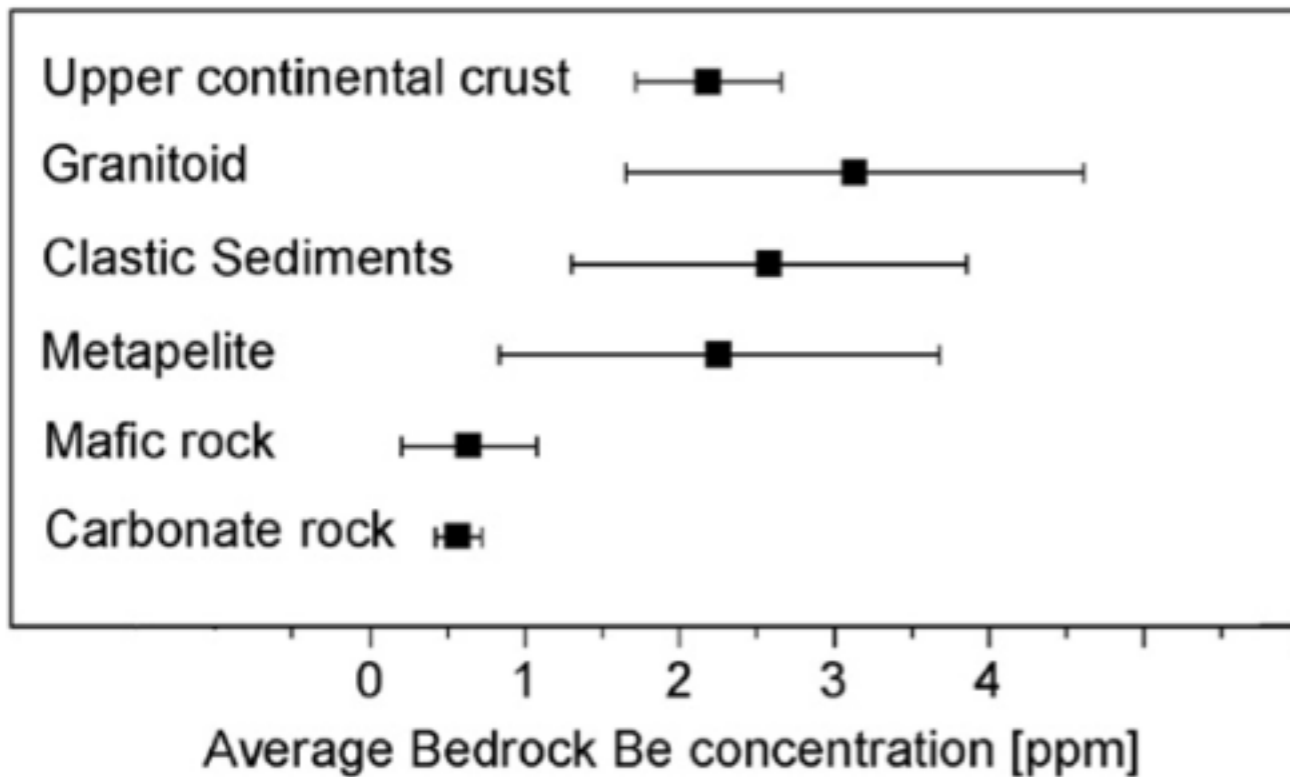


(similar charge to radius ratio to Al^{3+})

“mineral” ^9Be

“reactive” ^9Be “dissolved” ^9Be

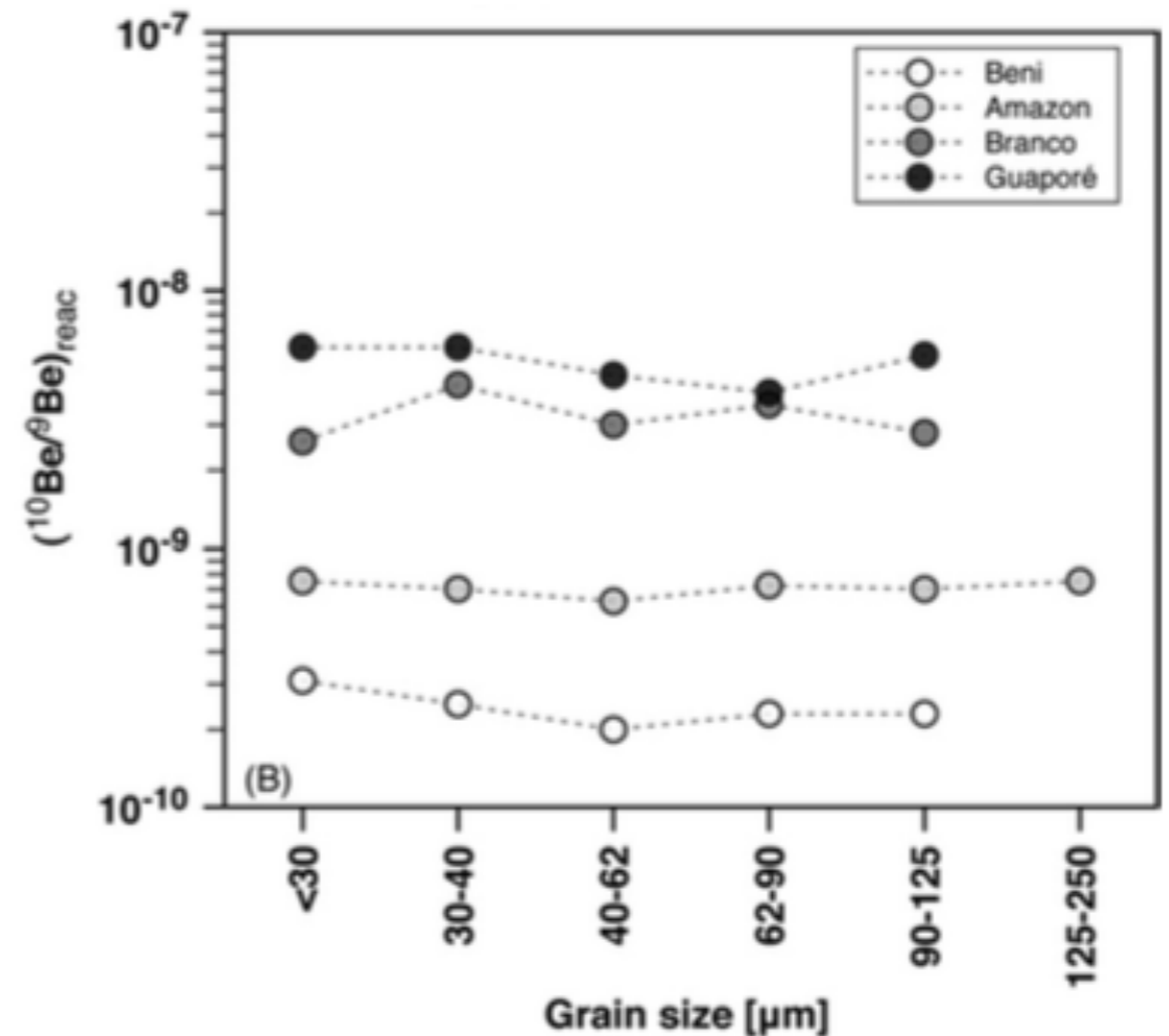
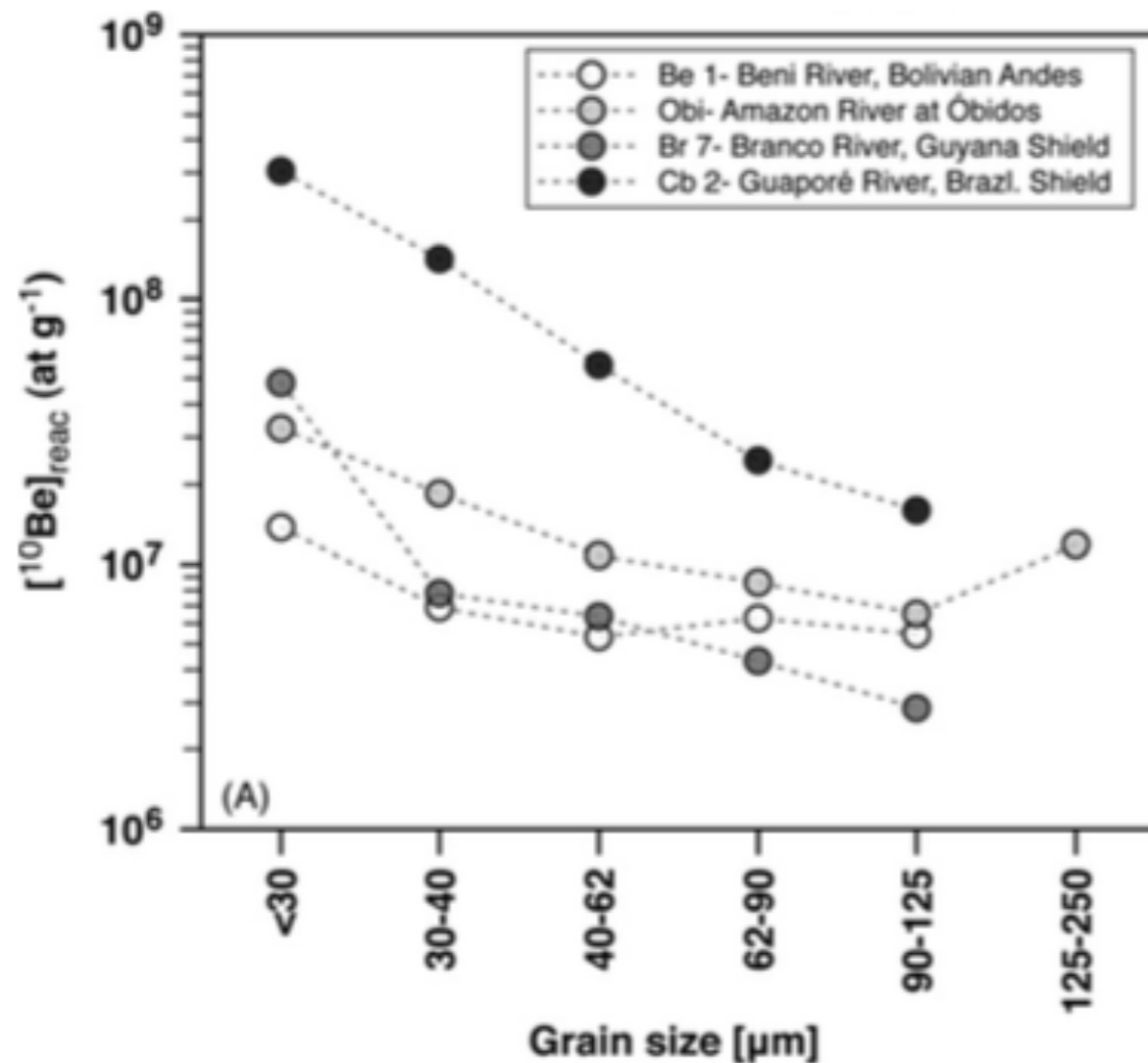
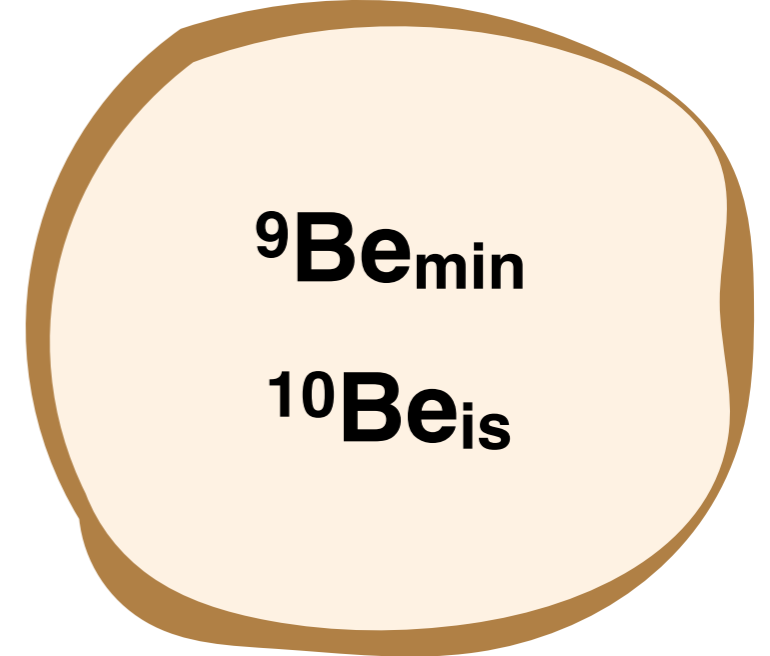
“parent” or “total” ^9Be



background, part 1. $^{10}\text{Be}/^9\text{Be}$ dynamics, sources

$$\frac{^{10}\text{Be}_{\text{met}}}{^9\text{Be}_{\text{reactive}}} \propto ^{10}\text{Be}_{\text{is}}$$

$^{10}\text{Be}_{\text{met}}$ $^9\text{Be}_{\text{reactive}}$

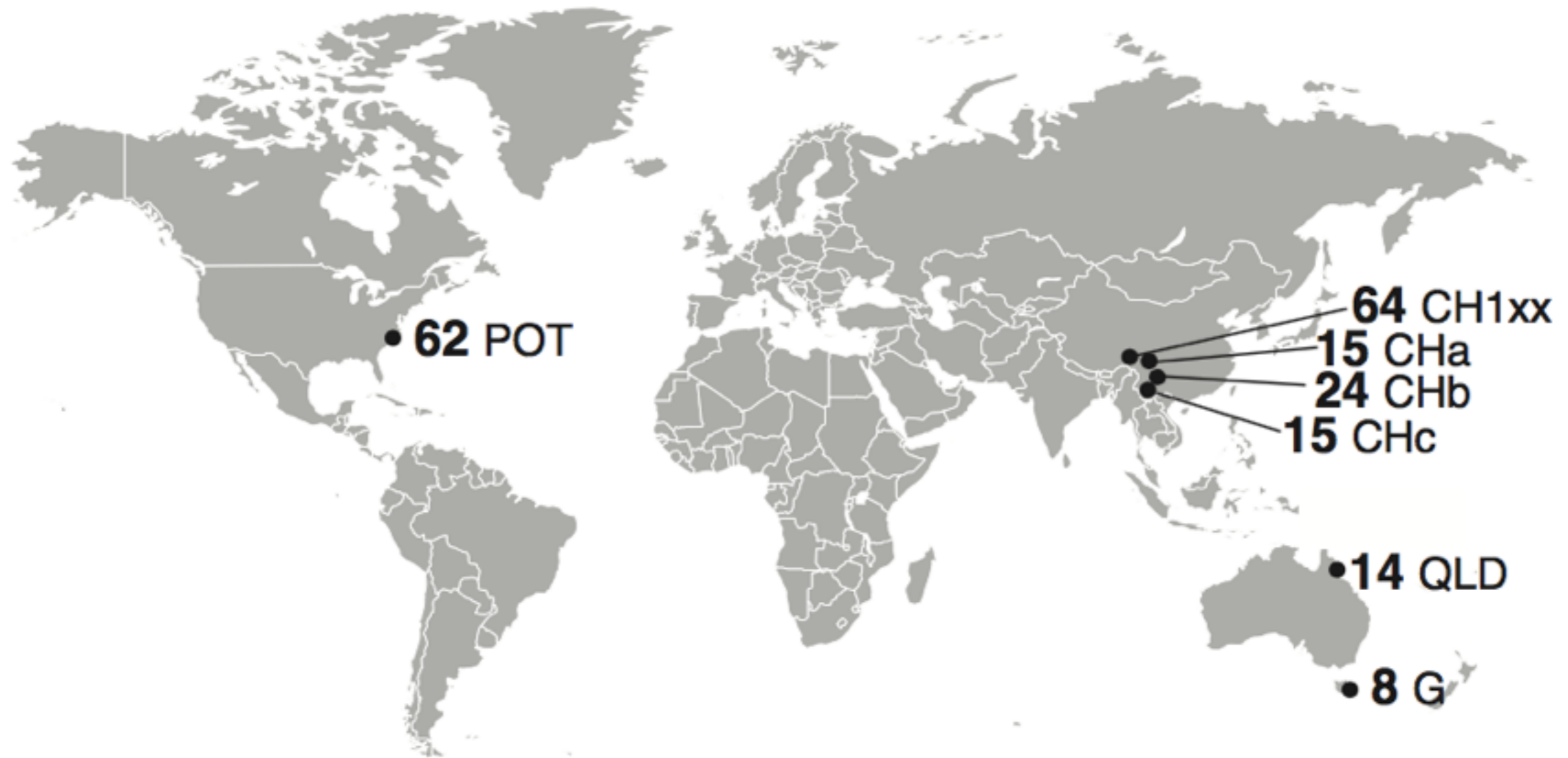


part 1. motivation

- samples with known meteoric and *in situ* ^{10}Be
 - can look at regional trends and trends across diverse study areas
- unique opportunity to compare *in situ* ^{10}Be , meteoric ^{10}Be , ^9Be , total grain coating composition, and basin characteristics



available samples



202 fluvial sediment samples

(72 soil samples, 222 glacial lake varve samples, 60 suspended sediment samples)

methods, part 1. Extracting ^9Be and method development

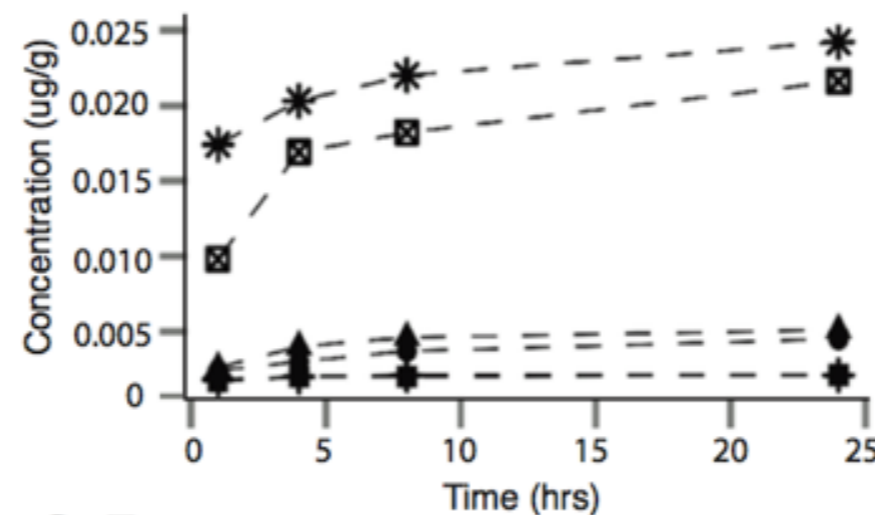
	QLD-5		CPA-12		Homogenized varve sample	
	6M	3M	6M	3M	6M	3M
1 hr	A1	B1	C1	D1	E1	F1
3 hrs	A2	B2	C2	D2	E2	F2
8 hrs	A3	B3	C3	D3	E3	F3
24 hrs	A4	B4	C4	D4	E4	F4
24 hrs (replicate)	A5	B5				

- testing 3 samples types with 2 acid treatments over 4 extraction times
- measured **Be**, Fe, Mg, Mn, Al, Si, Ti, Na, and K on Inductively Coupled Plasma Optical Emission Spectrometer

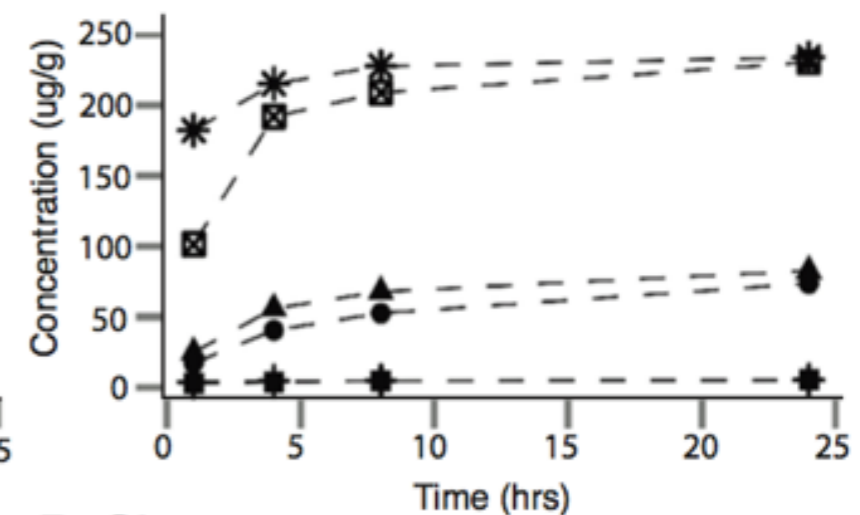
- **final method:**
0.250 g, 2 mL
6M HCl, 24
hours extraction
in heated
ultrasonic bath

●	CPA-12 3M
▲	CPA-12 6M
■	QLD-5 3M
+	QLD-5 6M
⊠	varve 3M
*	varve 6M

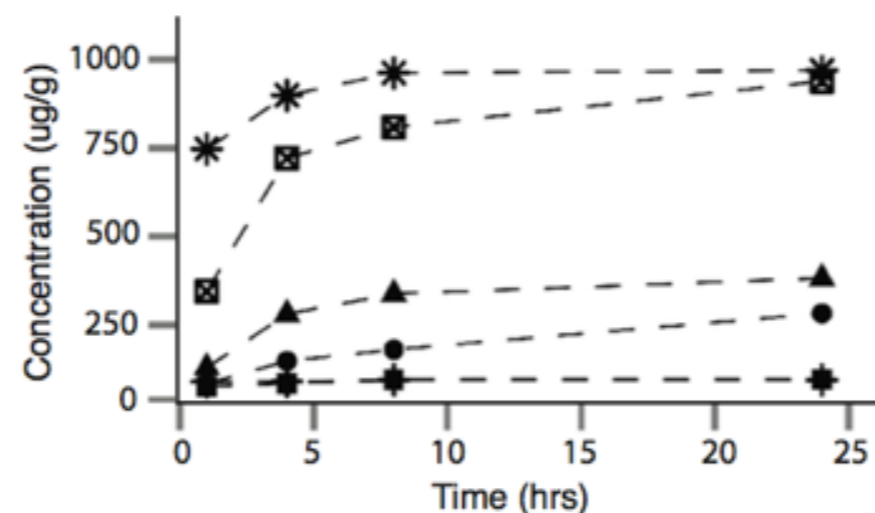
A. Be



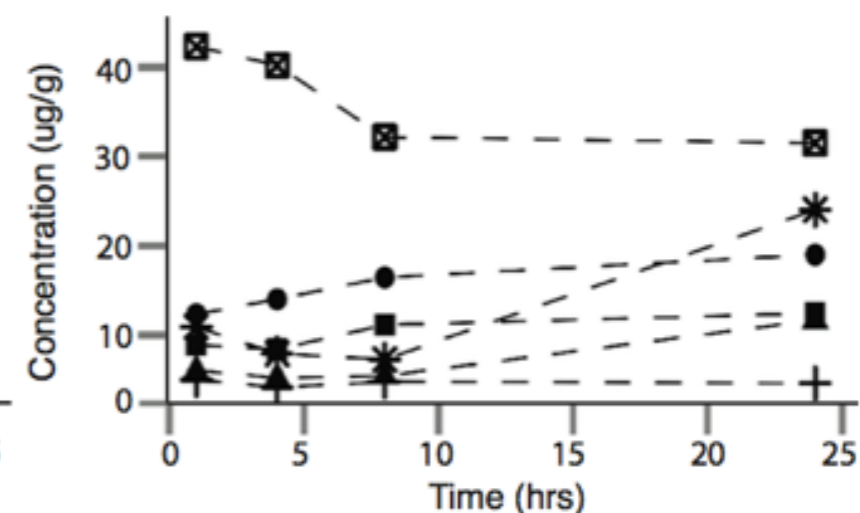
B. Mg



C. Fe



D. Si



methods, part 1. Total grain digest (n = 140)

residual sediment

step 1: DI rinse

rinsed and centrifuged (x3), dried overnight

step 2: HNO₃ digest

1:1 HNO₃ followed by aliquots of conc. HNO₃, heated at 95

step 3: H₂O₂ digest

1:1 H₂O₂, followed by aliquots of conc. H₂O₂, heated at 85

organic fraction

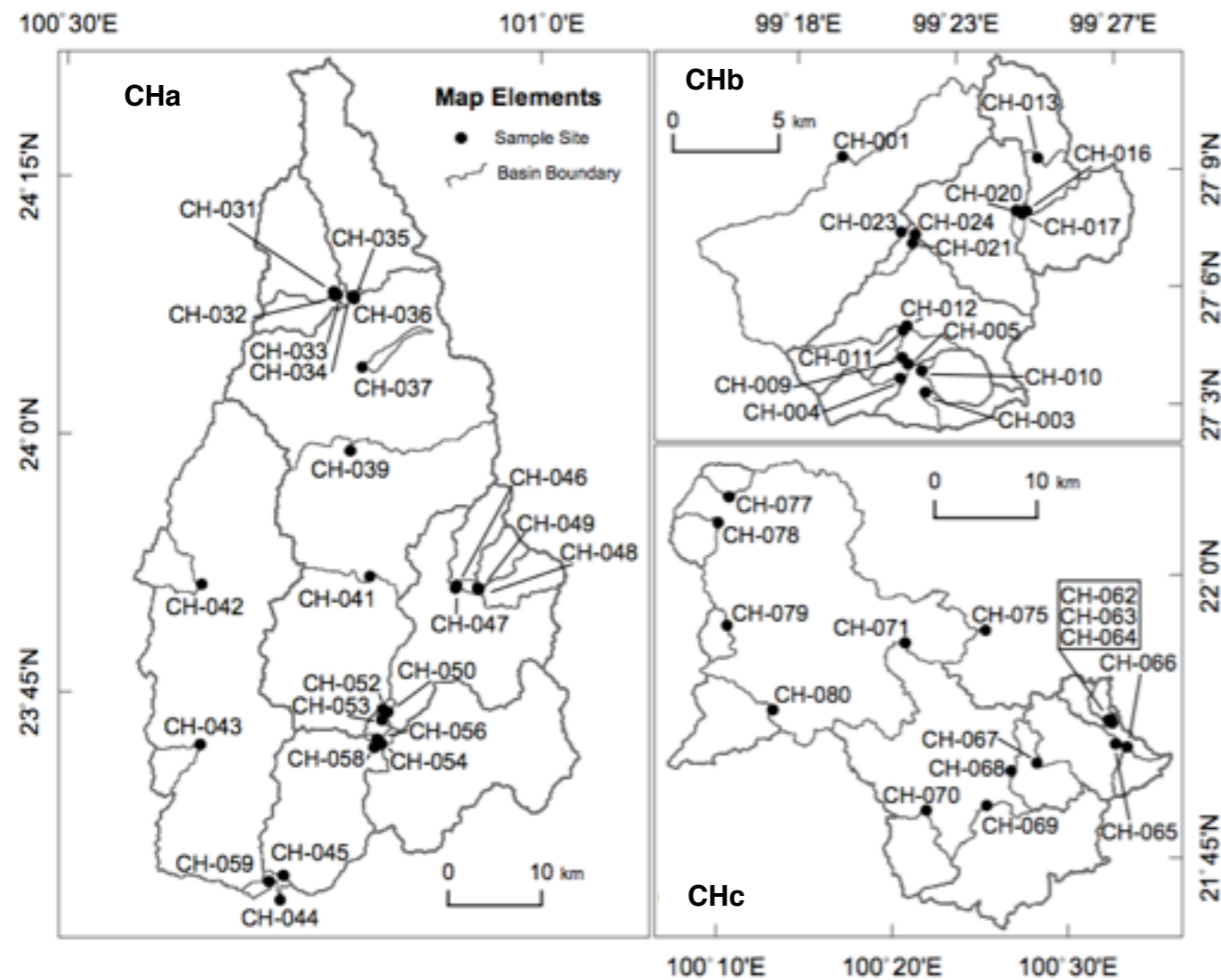
silicates

step 4: HClO₄, H₂SO₄, HF digest

cocktail of HClO₄, H₂SO₄, and HF digested overnight at 105, evaporated to dryness at 110, evaporated at 230 ~3 hrs.

diluted solution for ICP-OES

methods, part 1. Calculating basin parameters



mean basin slope
total basin relief
mean elevation
mean latitude
mean annual precipitation

latitude and precipitation used to
calculate mean basin **meteoric ^{10}Be**
delivery rates

modified from Nielson (2016). Using long and short-lived sediment associated isotopes to track erosion and sediment movement through rivers in Yunnan, SW China. (MS thesis)

Methods, part 1. In Review

What I was given:

- *in situ* ^{10}Be
- meteoric ^{10}Be
- calculated *in situ* ^{10}Be -derived denudation rates

What I measured:

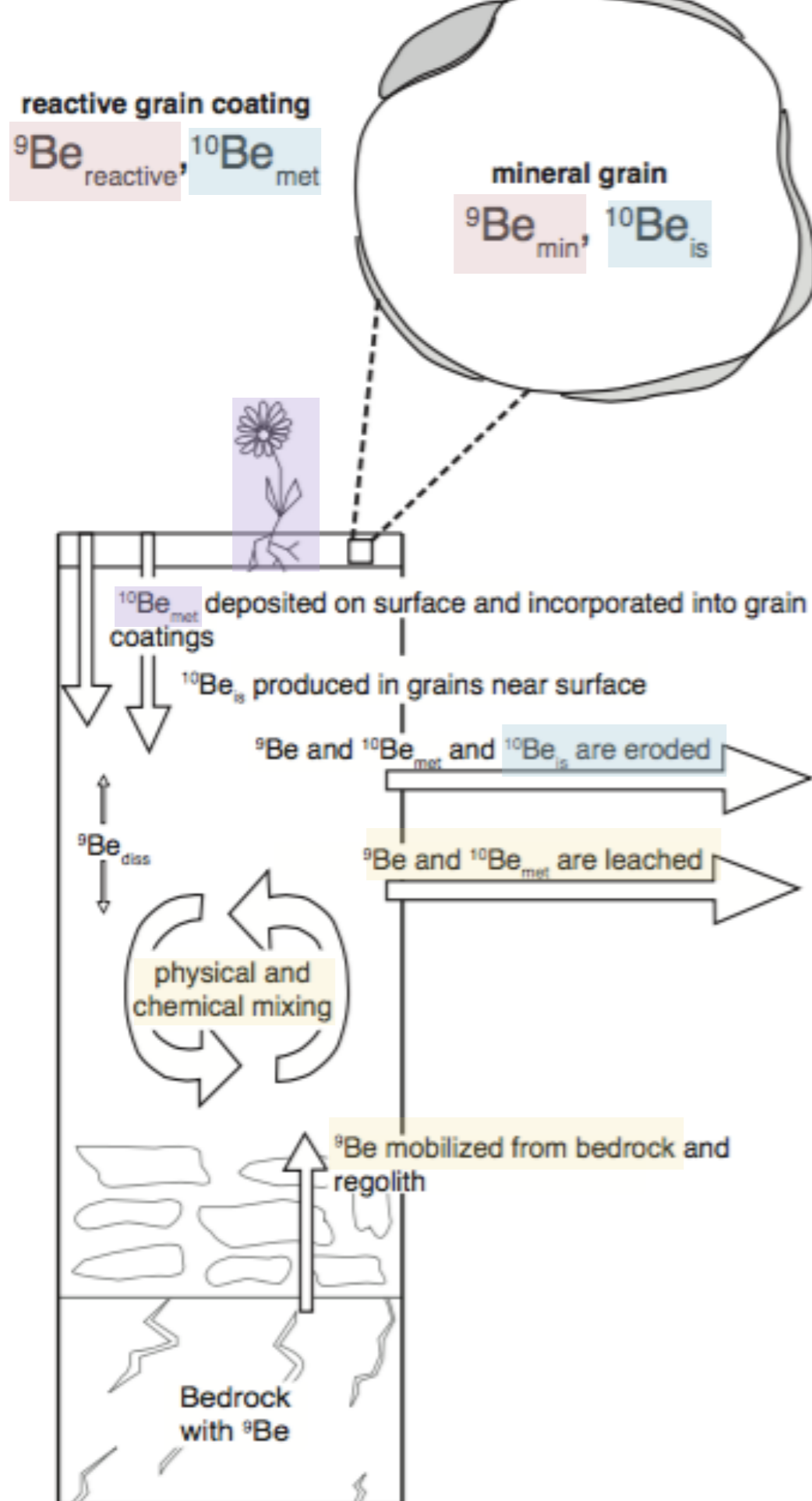
- reactive ^9Be
- mineral ^9Be

What I calculated:

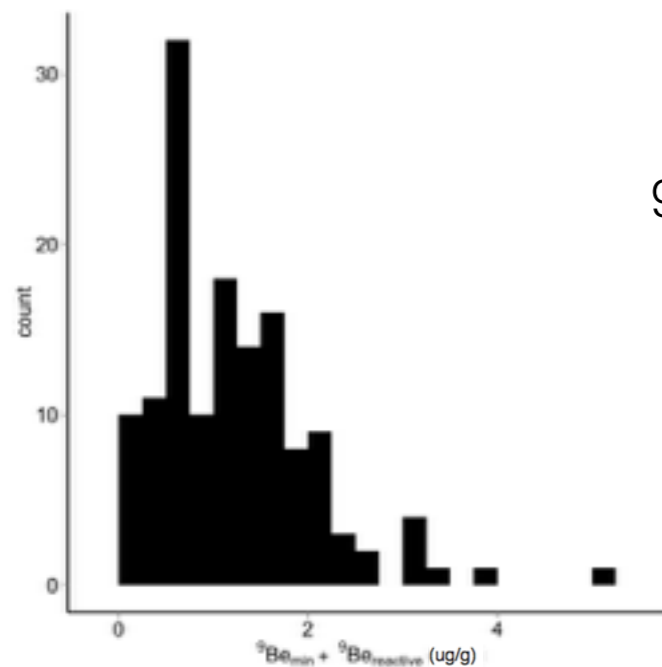
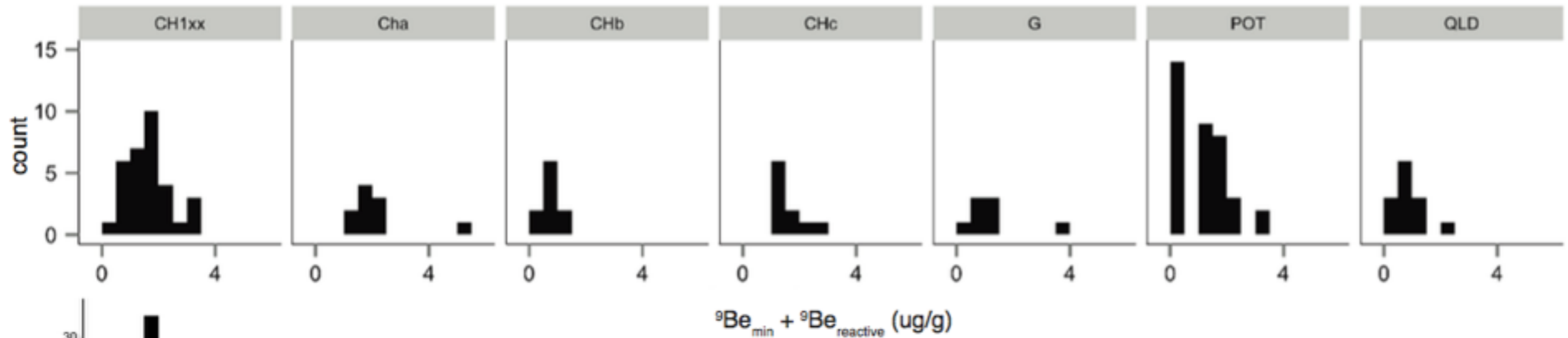
- basin characteristics, meteoric ^{10}Be delivery rates

What I want to learn more about:

- ^9Be and parent materials
- meteoric ^{10}Be and ^9Be mixing
- relative importance of controls on ^9Be and meteoric ^{10}Be concentrations in grain coatings



results: part 1. ^9Be abundances



$^9\text{Be}_{\text{min}} + ^9\text{Be}_{\text{reactive}}$ range all samples: 0.10-5.12 ug/g

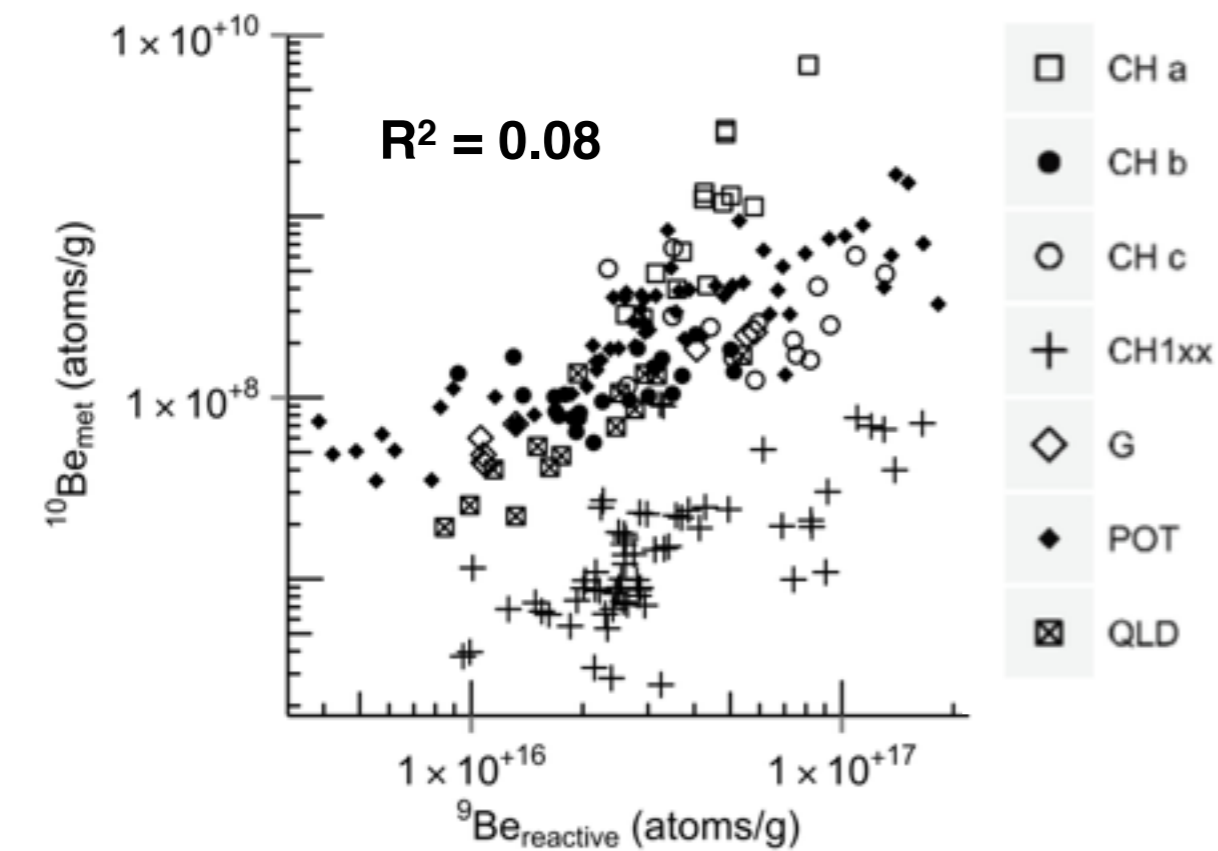
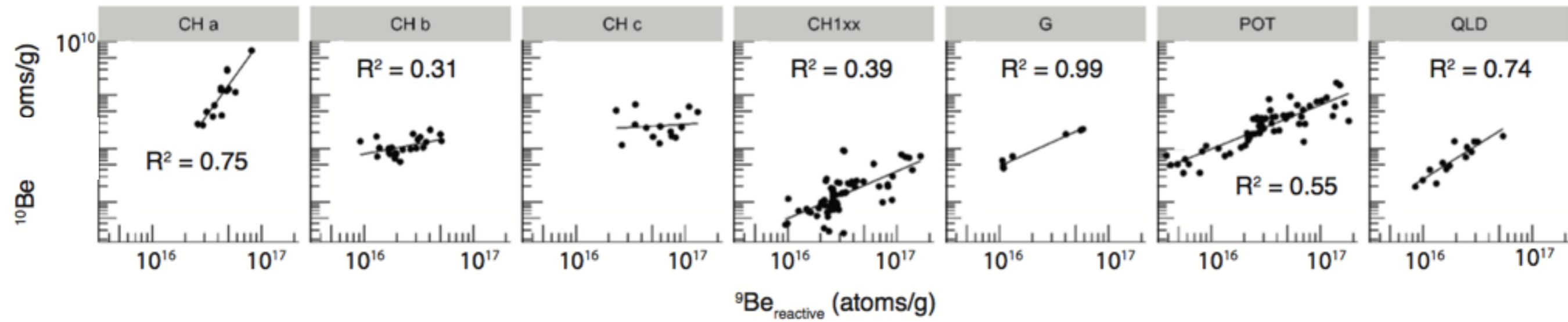
mean: 1.23 ± 0.82 ug/g

(mean crustal abundance = 2.50 ug/g)

$^9\text{Be}_{\text{reactive}}$

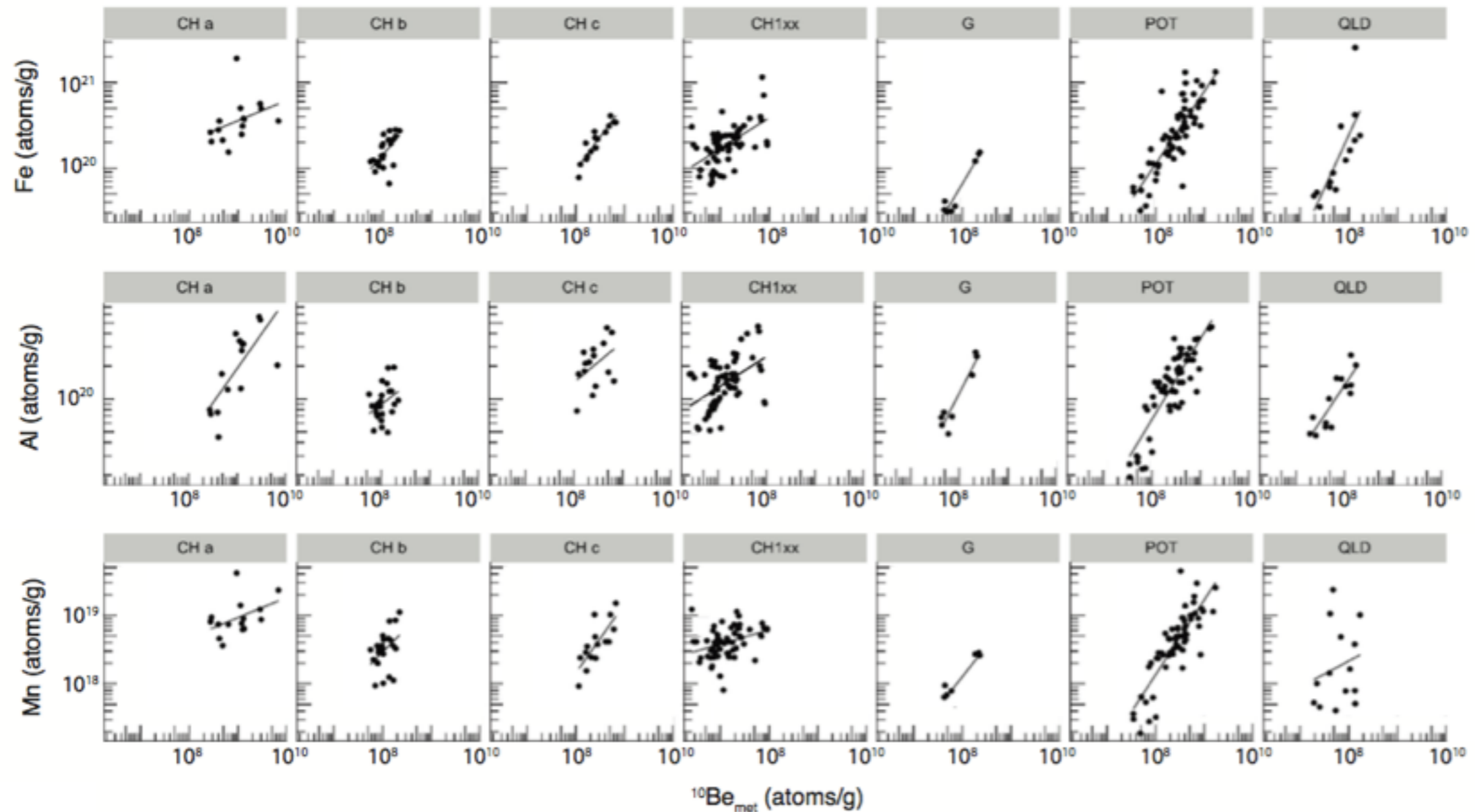
$^9\text{Be}_{\text{min}}$

results: part 1. ^9Be and meteoric ^{10}Be are correlated



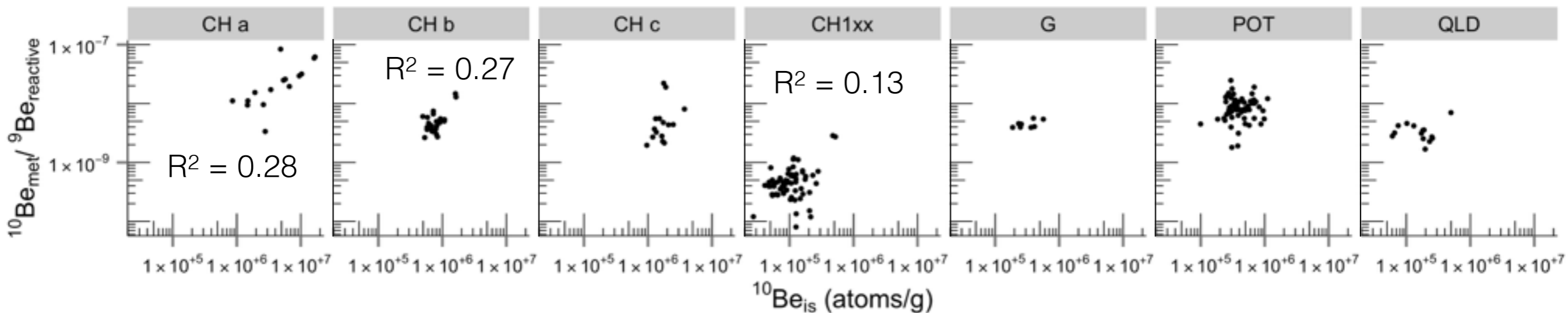
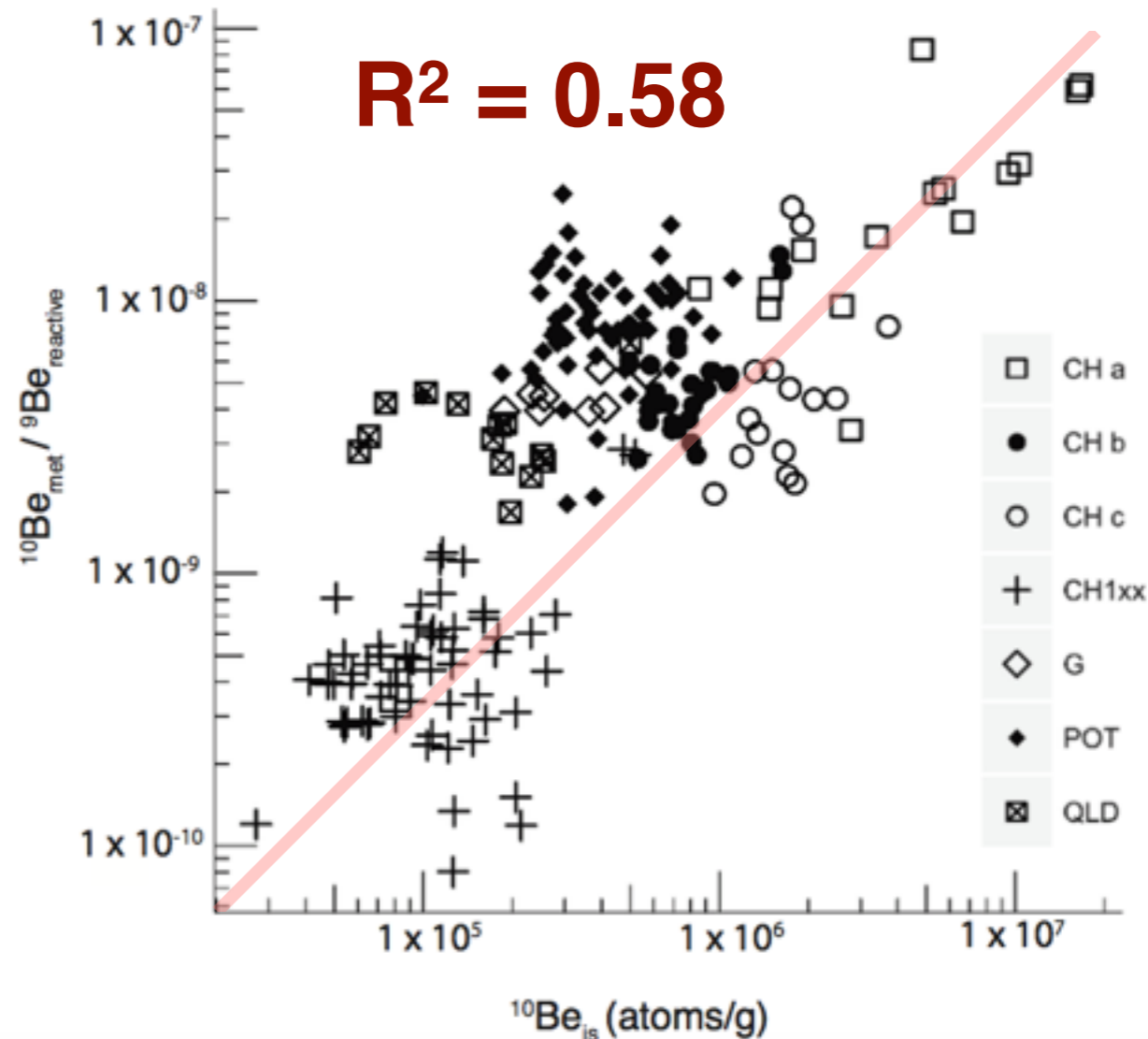
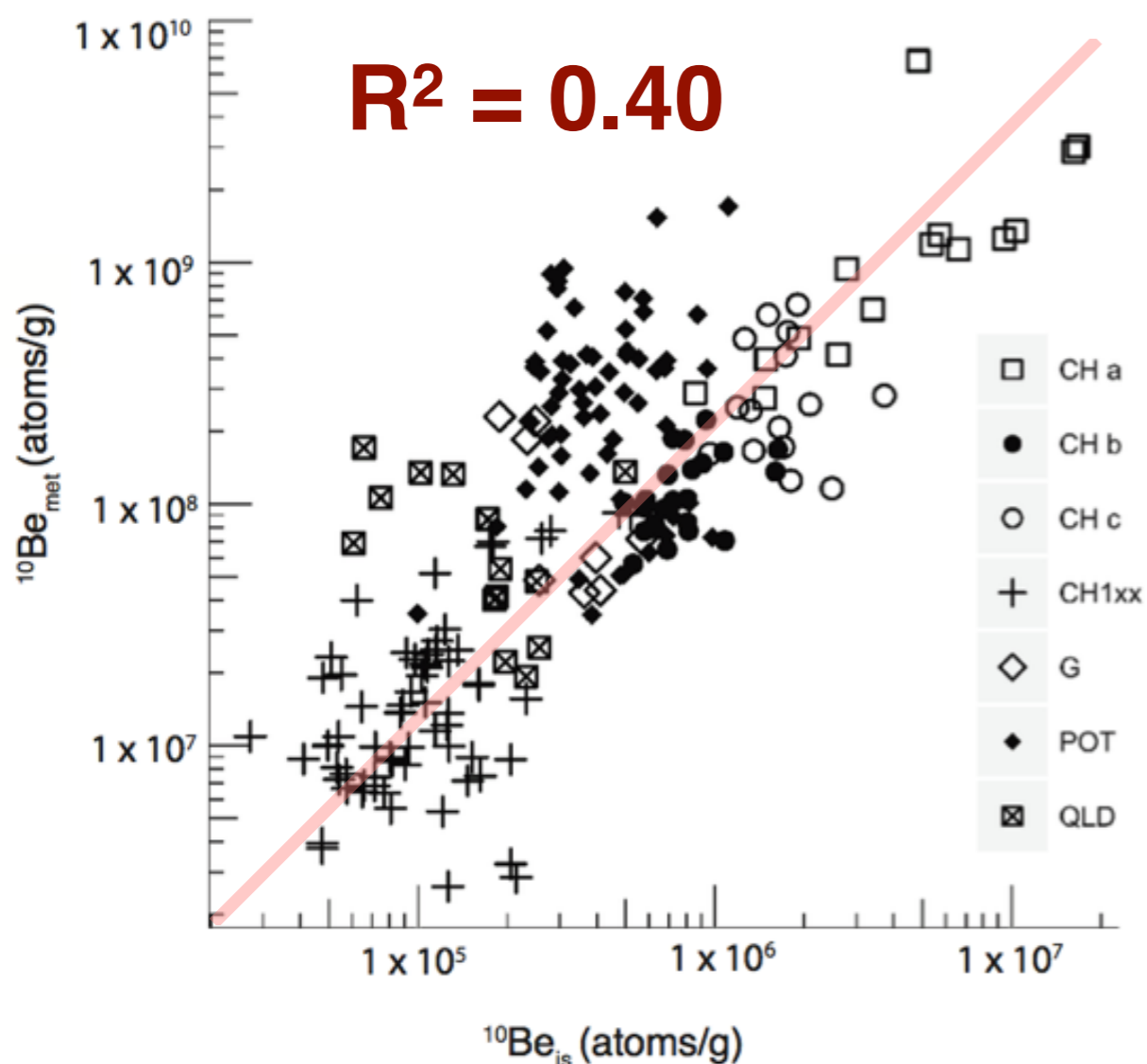
- correlations denoted with R^2 have p value < 0.05
- only site with non-significant correlation is CHc
- weak correlation considering all samples

results: part 1. ^9Be and meteoric ^{10}Be correlated to Al, Mn, and Fe in study areas

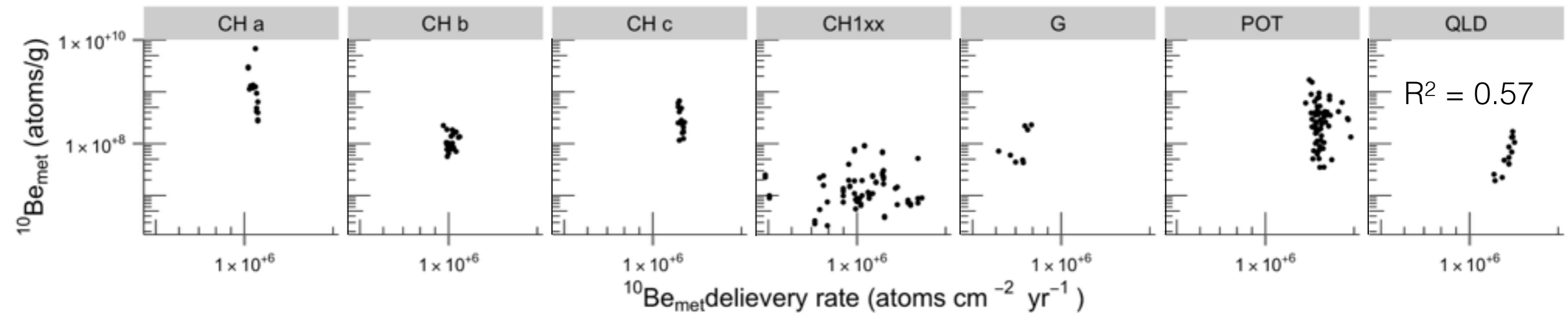


- strong correlation in many study areas; no correlation in others
- Al, Fe, and Mn make up the largest percentage by mass of HCl-extractable materials

results: part 1. meteoric $^{10}\text{Be}/^9\text{Be}$ correlated to *in situ* ^{10}Be

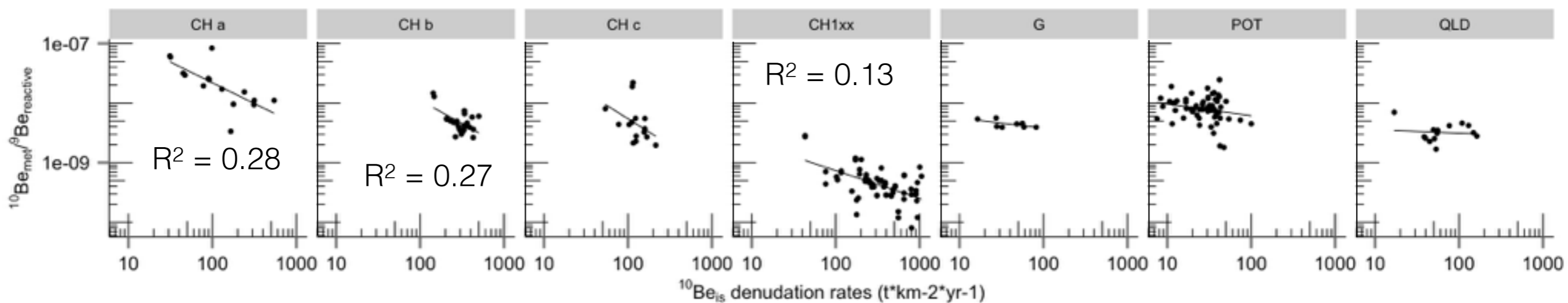


results: part 1. meteoric ^{10}Be not correlated to $^{10}\text{Be}_{\text{met}}$ delivery rates



no strong correlation across all samples

results: part 1. meteoric $^{10}\text{Be}/^9\text{Be}$ not correlated to denudation rates



no strong correlation across all samples

results: part 1. not many significant correlations between Be isotopes and basin characteristics

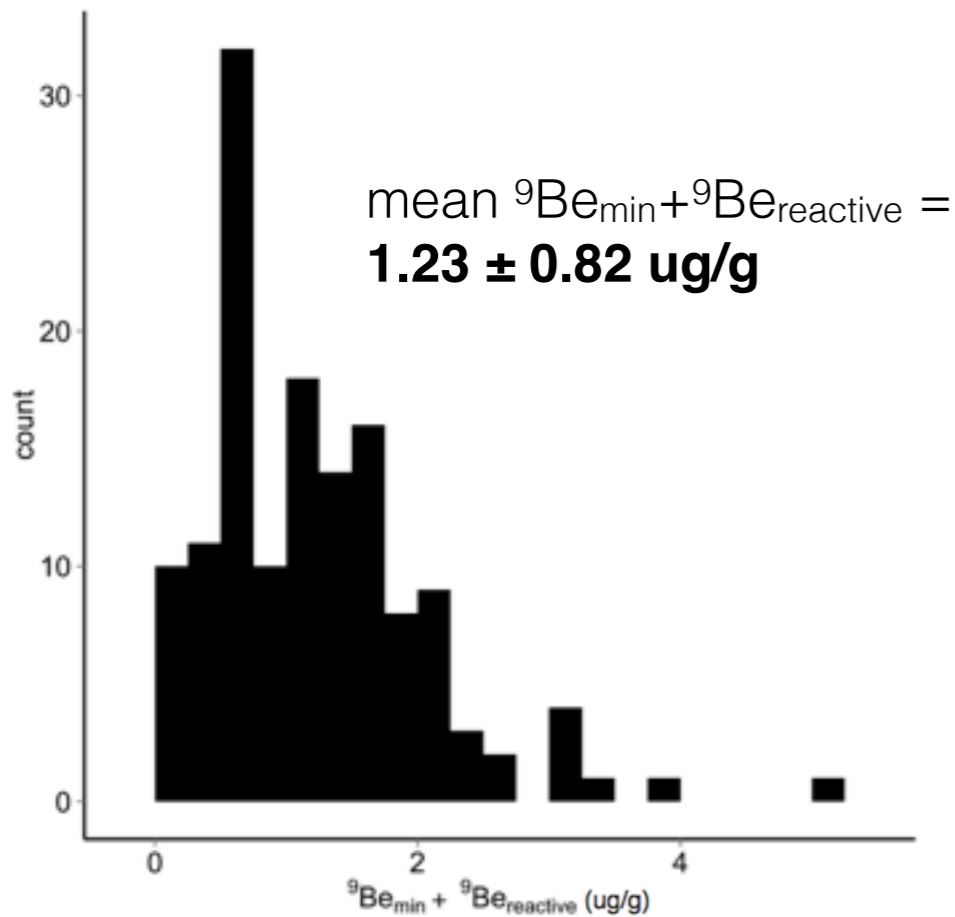
Table 3.

R² and p values of correlations between Be isotopes concentrations and MAP, mean basin slope, and total relief for each study area and for all samples.

study ID	n	basin parameter	¹⁰ Be _{is}		¹⁰ Be _{met} / ⁹ Be _{reactive}		¹⁰ Be _{is} denudation rate		¹⁰ Be _{met} / ⁹ Be _{reactive} -derived denudation rate ^d	
			R ²	p	R ²	p	R ²	p	R ²	p
All samples	202	MAP	<0.01	0.53	0.03	0.01	0.01	0.18	<0.01	0.45
		mean basin slope	<0.01	0.46	0.03	0.01	0.46	<0.01	0.17	<0.01
		total relief	0.02	0.03	0.11	<0.01	0.55	<0.01	0.42	<0.01
		mean elevation	0.08	0.07	<0.01	0.62	0.43	<0.01	0.22	<0.01
		mean latitude	0.01	0.25	0.03	0.01	0.10	<0.01	0.05	<0.01
		basin size	0.01	0.09	0.04	0.01	0.33	<0.01	0.24	<0.01

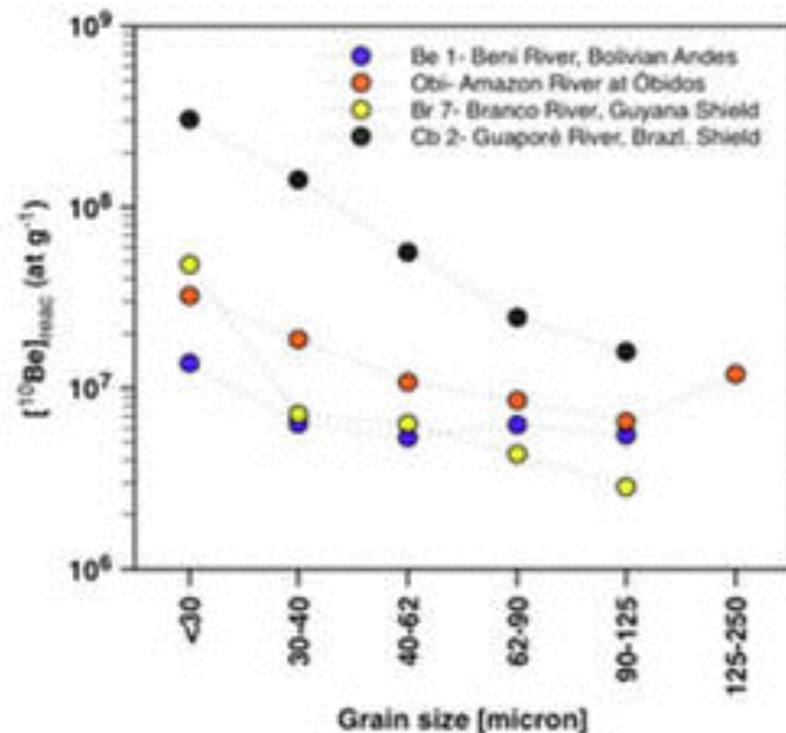
- correlations in bold print have R² > 0.30 and p value < 0.05
- significant correlations between *in situ* denudation rates and slope, total relief, mean elevation, and basin size (positive correlations)
- not strong and significant correlations between meteoric ¹⁰Be/⁹Be or *in situ* ¹⁰Be and basin parameters

discussion, part 1. ^9Be concentrations in grains lower than bedrock



- mineral and reactive ^9Be concentrations lower than mean crustal abundance ($2.5 \text{ } \mu\text{g/g}$)
 - sand sized sediments collected ($250\text{-}850 \text{ } \mu\text{m}$)
 - ^9Be in dissolved phase

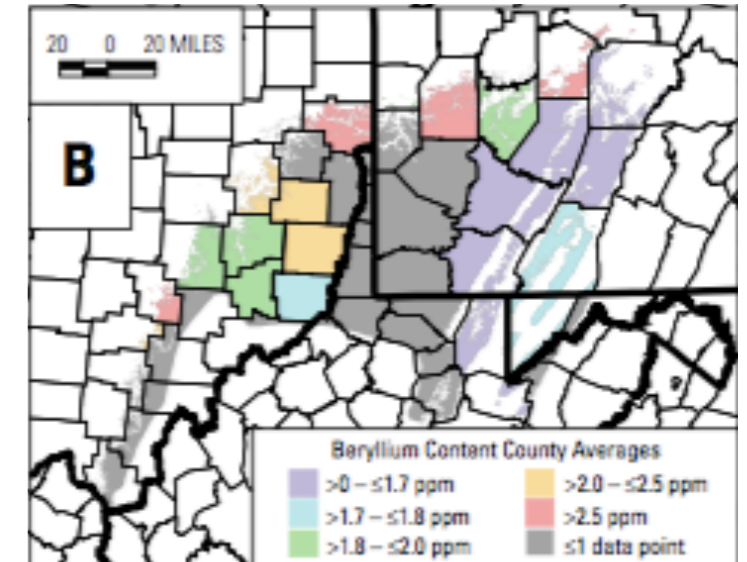
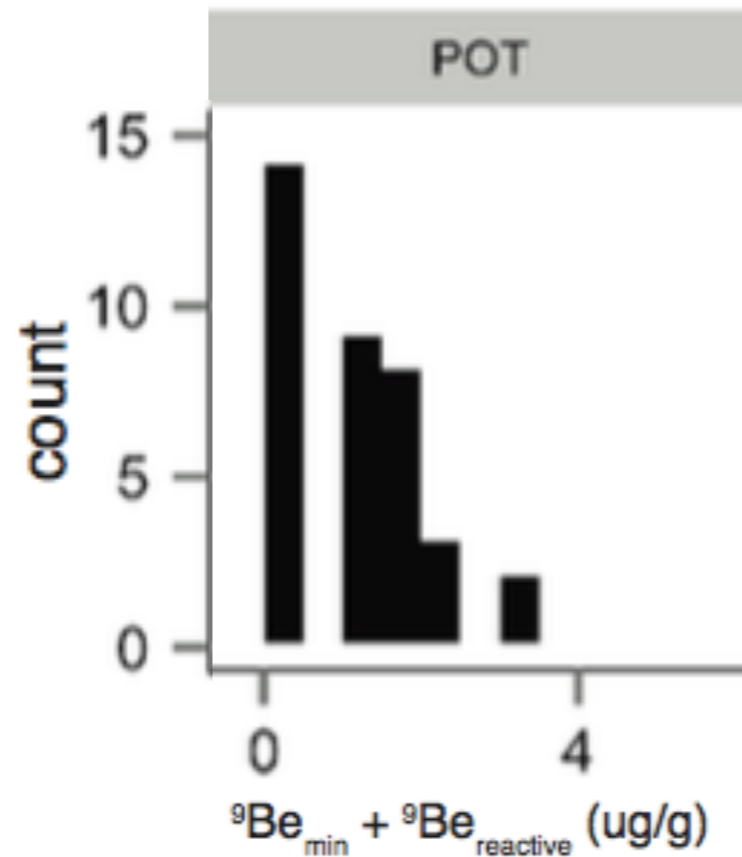
Sample	$f_{\text{diss}}^{^9\text{Be}}$	$f_{\text{react}}^{^9\text{Be}}$	$f_{\text{min}}^{^9\text{Be}}$	$f_{\text{react}}^{^9\text{Be}} + f_{\text{diss}}^{^9\text{Be}}$
Amazon at Macapa/Obidós	0.029	0.23	0.74	0.26
Solimoes at Manaus	0.018	0.11	0.87	0.13
Negro at Manaus	0.65	0.29	0.06	0.94
Amazon Andean Rivers	0.002	0.29	0.71	0.29
Beni	0.001	0.31	0.69	0.31



discussion, part 1. wide range of ^9Be reactive concentrations

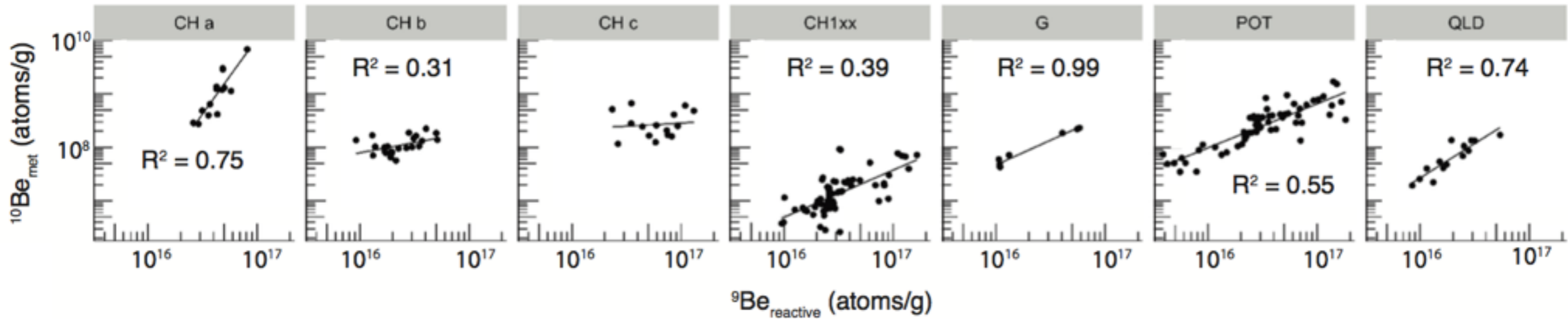


Figure 8. Photograph of the Upper Freeport coal bed in Pennsylvania. Person is pointing to the upper contact of the coal bed. Note the overlying sandstone. (Photograph courtesy of James Shaulis, Pennsylvania Bureau of Topographic and Geologic Survey.)



- Upper Freeport coal bed enriched in Be relative to sediment: mean concentration = $1.80 \pm 0.81 \mu\text{g/g}$, max concentration = $5 \mu\text{g/g}$
- higher reactive ^9Be concentrations in samples from north branch of Potomac River than main stem
- ^9Be in parent materials influences ^9Be in grain coatings, even in regional studies

discussion, part 1. meteoric ^{10}Be and ^9Be correlated in grain coatings



Terraced agriculture

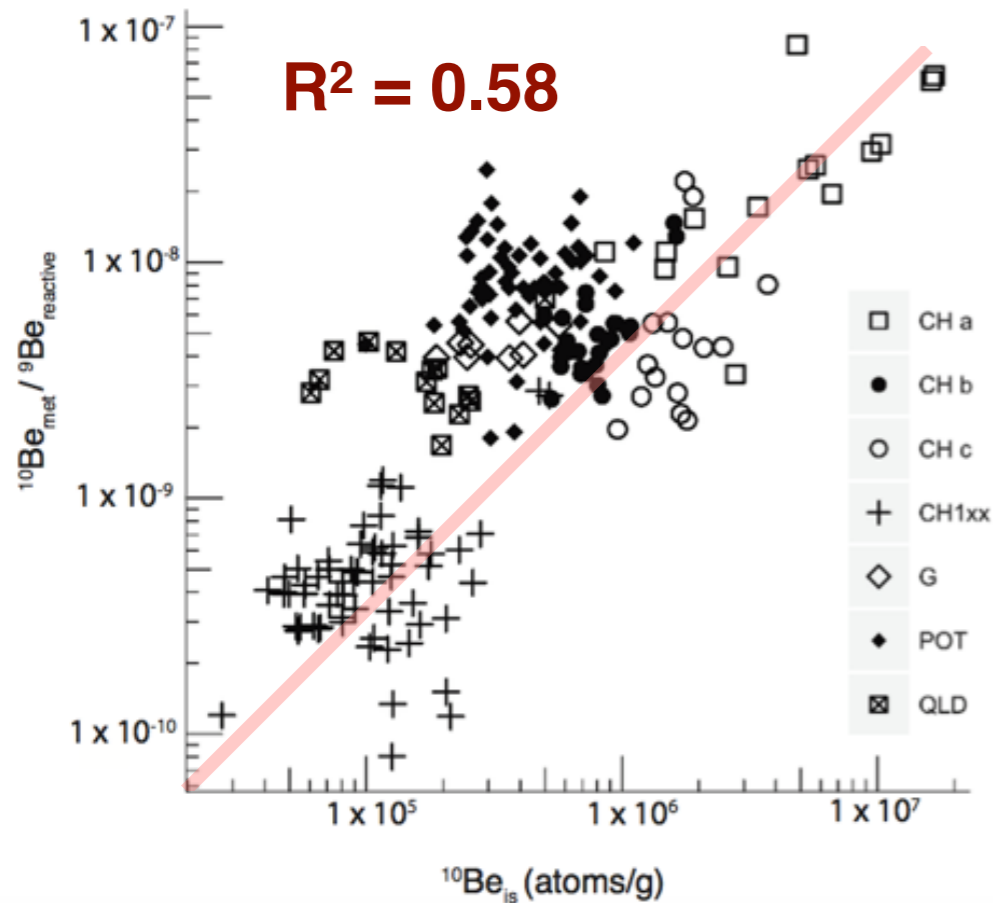


- correlation suggests $^{10}\text{Be}_{\text{met}}$ deposited on the surface and ^9Be weather from buried bedrock are mixed in grain coatings
- exception = CHc study area
- anoxia in flooded hillslopes prevents biotic mixing

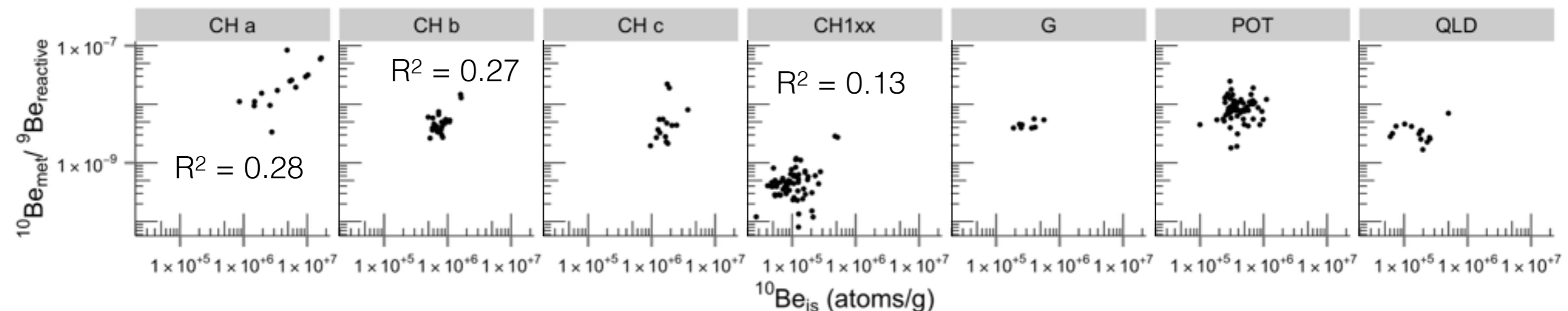
CH-079

Parent Basin: 11
Collection Date: 6/8/13
Latitude: 21.958 Longitude: 100.179
Sample Type: RS
Additional Notes: Small tributary of N. arm of basin 11 with anabranching channel.
Sample collected from immediately above small diversion structure.

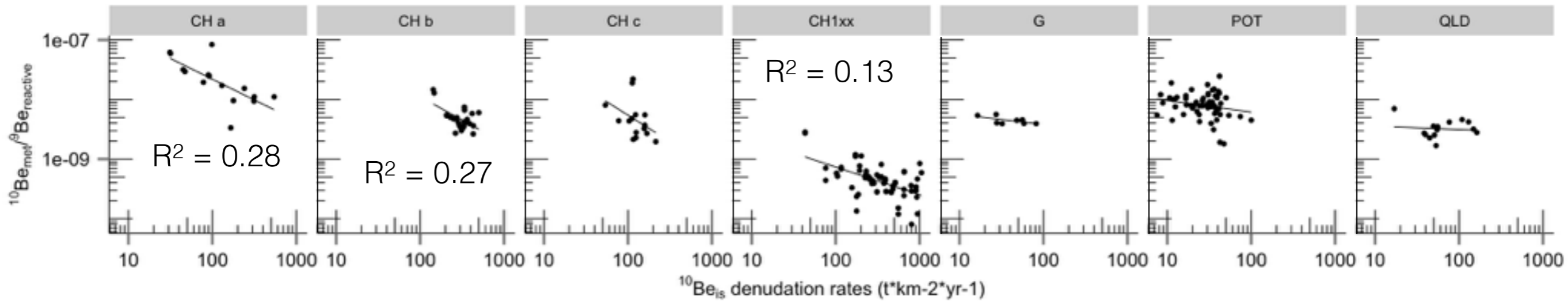
discussion, part 1. stronger correlation between meteoric $^{10}\text{Be}/^9\text{Be}$ ratios and $^{10}\text{Be}_{\text{is}}$ than $^{10}\text{Be}_{\text{met}}$ alone



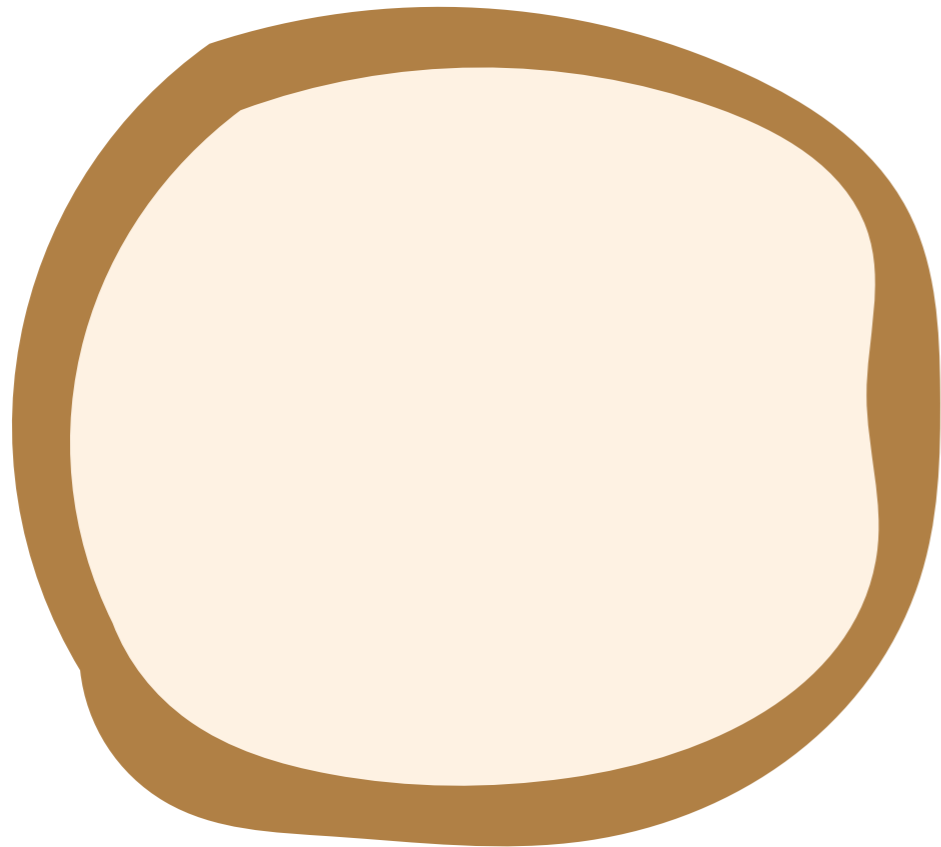
- significant correlation with $^{10}\text{Be}_{\text{is}}$ for all data
- weak correlation (or none at all) when considering regional data
- biological remobilization, leaching processes influence meteoric $^{10}\text{Be}/^9\text{Be}$
- these effects obscure correlations when only considering $^{10}\text{Be}_{\text{is}}$ that span a few orders of magnitude



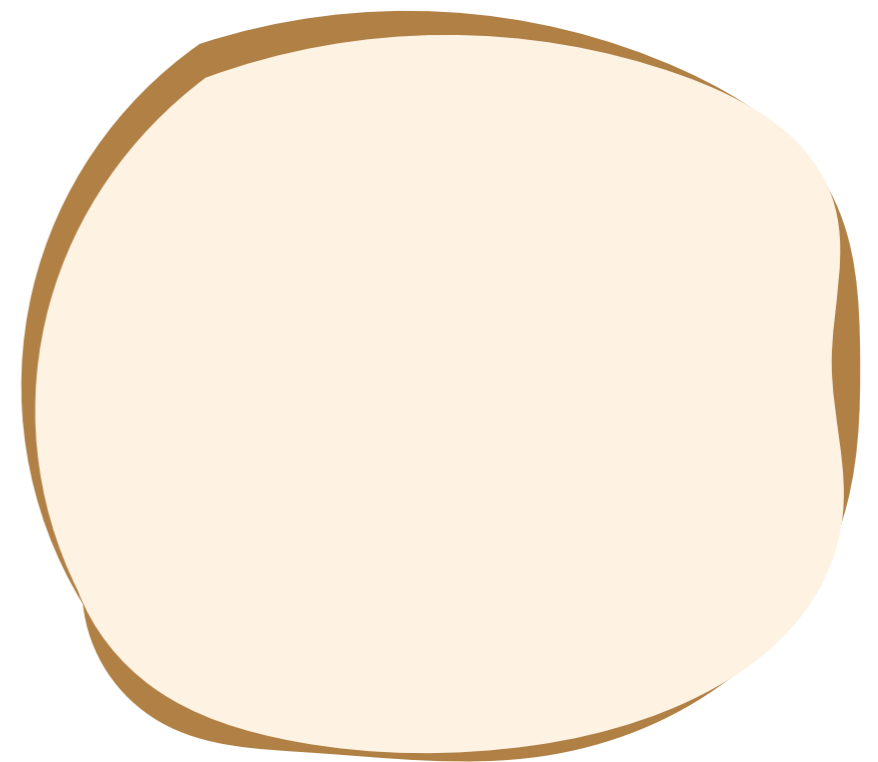
discussion, part 1. $^{10}\text{Be}_{\text{met}}/^{9}\text{Be}$ ratios not correlated to denudation rates



more time in soil profile \rightarrow more $^{10}\text{Be}_{\text{met}}$ and ^9Be accumulated in grain coatings



more leaching \rightarrow less $^{10}\text{Be}_{\text{met}}$ and ^9Be in grain coatings



- indicates influence of remobilization and leaching

discussion, part 1. processes that decouple grains and grain coatings



- acidic soil environments; leaching
- anoxic environments; leaching
- physical abrasion

discussion, part 1. not many significant correlations between Be isotopes and basin characteristics

Table 3.

R² and p values of correlations between Be isotopes concentrations and MAP, mean basin slope, and total relief for each study area and for all samples.

study ID	n	basin parameter	¹⁰ Be _{is}		¹⁰ Be _{met} / ⁹ Be _{reactive}		¹⁰ Be _{is} denudation rate		¹⁰ Be _{met} / ⁹ Be _{reactive} -derived denudation rate ^d	
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All samples	202	MAP	<0.01	0.53	0.03	0.01	0.01	0.18	<0.01	0.45
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		mean latitude	0.01	0.25	0.03	0.01	0.10	<0.01	0.05	<0.01
		basin size	0.01	0.09	0.04	0.01	0.33	<0.01	0.24	<0.01

- confirms previous findings of correlation between *in situ* denudation rates and slope, total relief, mean elevation, and basin size (positive correlations)
- lack of correlations affirms suggestion that meteoric ¹⁰Be/⁹Be ratios are influenced by remobilization, grain size, and heterogeneous source materials

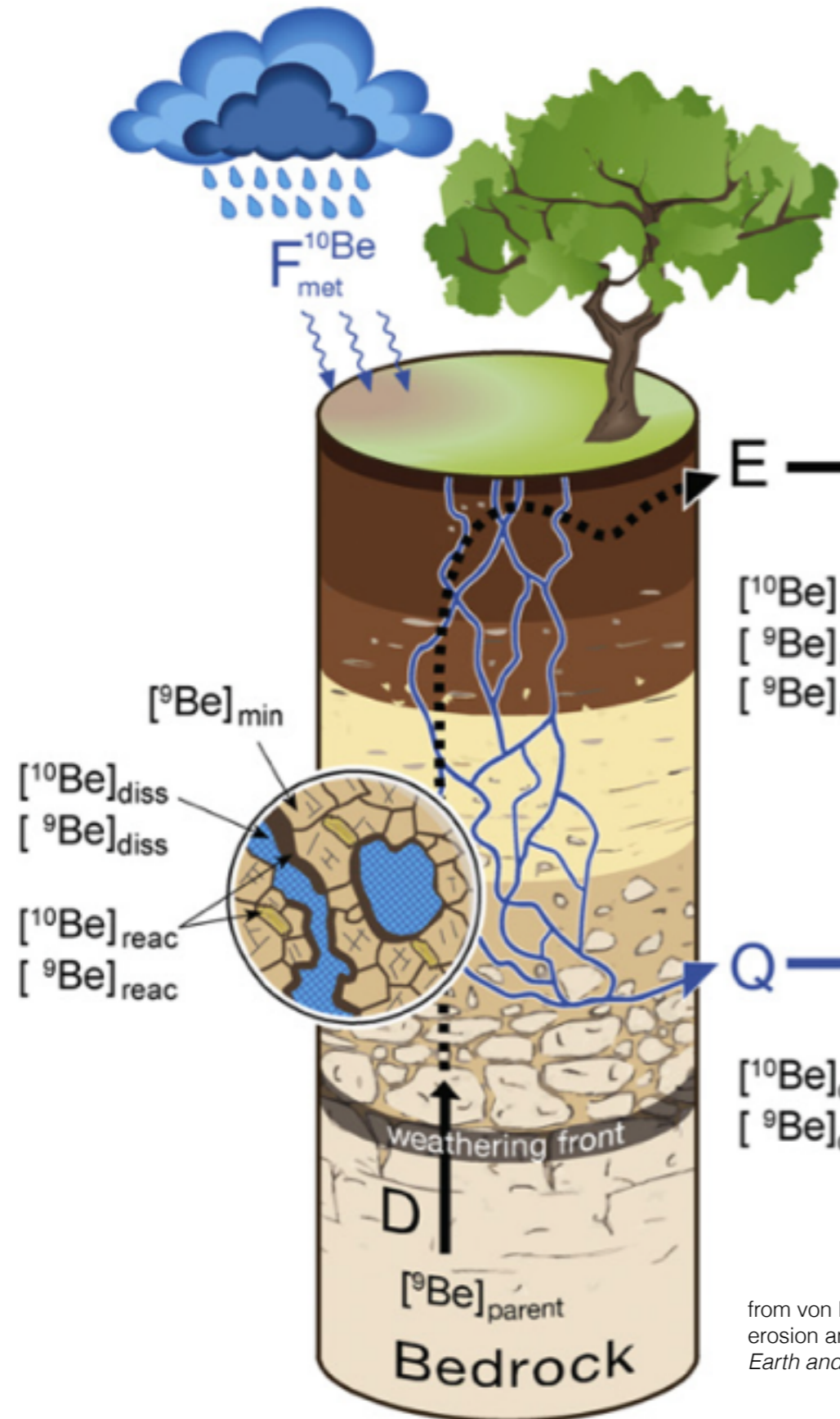
conclusions, part 1.

- total meteoric ^{10}Be stored in Al, Mn, and Fe dominated grain coatings
- spatial heterogeneities in ^{10}Be and ^9Be inputs influence concentrations in grain coatings.
- meteoric ^{10}Be and ^9Be well mixed in most grain coatings, but not in all study areas
- meteoric $^{10}\text{Be}/^9\text{Be}$ ratios are influenced by remobilization and leaching processes, not just denudation

part 2. meteoric $^{10}\text{Be}/^9\text{Be}$ derived denudation rates

- mass balance model that controls for heterogeneity in inputs, and calculates meteoric $^{10}\text{Be}/^9\text{Be}$ -derived denudation rates
 - assumptions needed to apply model
 - compare meteoric $^{10}\text{Be}/^9\text{Be}$ based denudation rates to *in situ* based denudation rates

background, part 2. mass balance model for $^{10}\text{Be}/^9\text{Be}$ denudation rates



$$D = \frac{F_{met}^{10}\text{Be}}{[{}^9\text{Be}]_{parent} * (f_{react}^{9}\text{Be} + f_{diss}^{9}\text{Be}) * \left(\frac{{}^{10}\text{Be}_{met}}{{}^9\text{Be}_{reactive}} \right)}$$

eq. 1

$$f_{react}^{9}\text{Be} + f_{diss}^{9}\text{Be}$$

fraction of ^9Be in the dissolved and reactive phase;
i.e. **f.factor**

from von Blanckenburg et al. (2012). Earth surface erosion and weathering from ^{10}Be (meteoric)/ ^9Be ratio. *Earth and Planetary Science*

methods, part 2. estimating constants

$$D = \frac{F_{met}^{10Be}}{[{}^9Be]_{parent} * f.factor * \left(\frac{{}^{10}Be_{met}}{{}^9Be_{reactive}} \right)} \quad \text{eq. 1}$$

mean ${}^{10}Be_{met}$ delivery rate for the study area calculated from empirical model based on latitude and MAP (Graly et al., 2011)

total measured ${}^{10}Be_{met}$ and acid-extractable 9Be for each sample

eq. 1'

$$f.factor = \frac{F_{met}^{10Be}}{[{}^9Be]_{parent} * D * \left(\frac{{}^{10}Be_{met}}{{}^9Be_{reactive}} \right)}$$

$D = in situ$ ${}^{10}Be$ -derived denudation rate

$$[{}^9Be]_{parent} = 2.5 \text{ ppm}$$

eq. 2

$$f.factor = \frac{{}^9Be_{reactive}}{{}^9Be_{reactive} + {}^9Be_{min}}$$

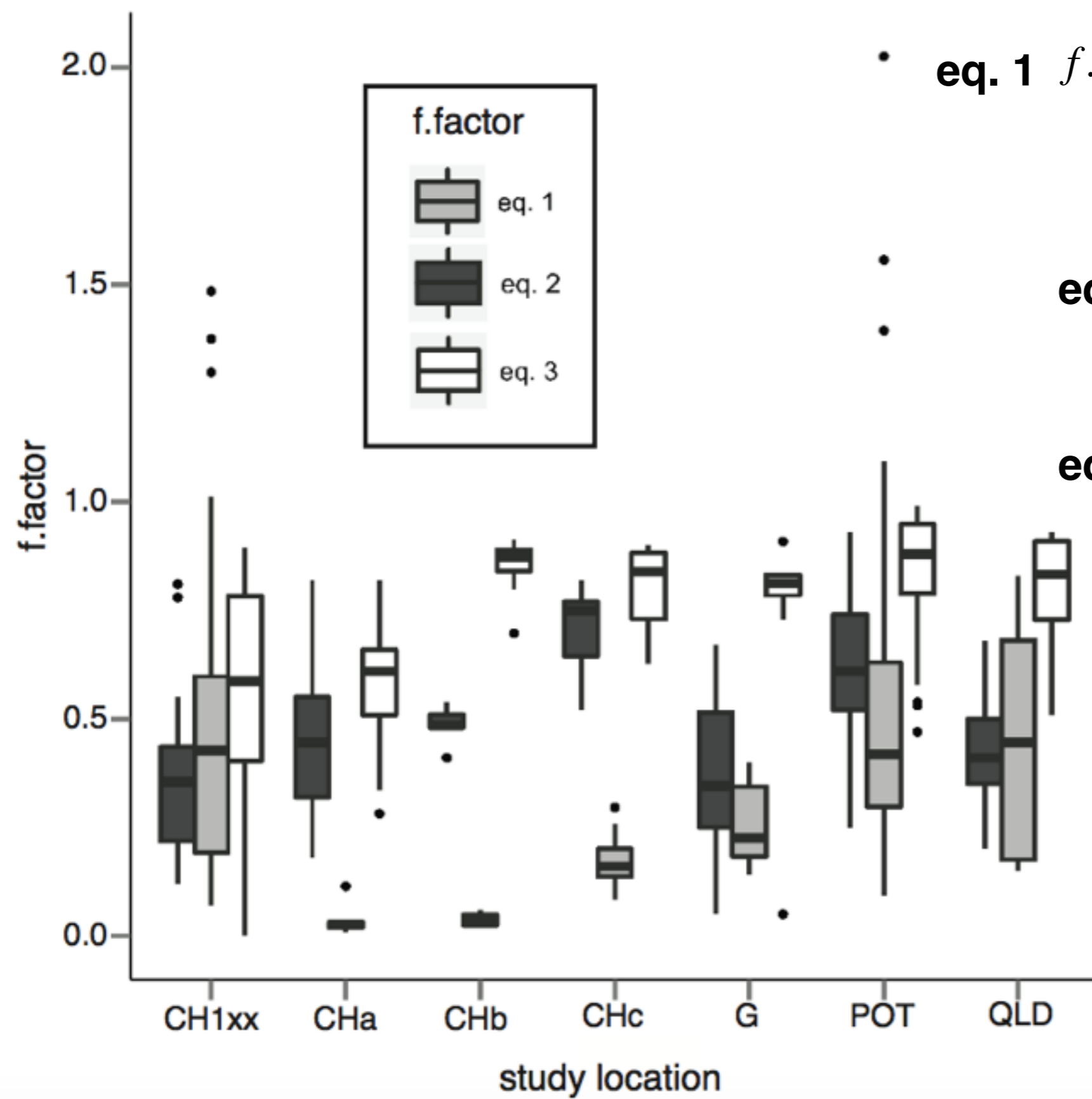
$$[{}^9Be]_{parent} = {}^9Be_{min} + {}^9Be_{reactive}$$

eq. 3

$$f.factor = \frac{{}^9Be_{reactive} + {}^9Be_{diss}}{2.5}$$

$$[{}^9Be]_{parent} = 2.5 \text{ ppm} = {}^9Be_{min} + {}^9Be_{reactive} + {}^9Be_{diss}$$

results: part 2. methods of calculating f.factor do not agree



eq. 1 $f.factor = \frac{F_{met}^{10Be}}{[{}^9Be]_{parent} * D * \left(\frac{{}^{10}Be_{met}}{{}^9Be_{reactive}} \right)}$

eq. 2 $f.factor = \frac{{}^9Be_{reactive}}{{}^9Be_{reactive} + {}^9Be_{min}}$

eq. 3 $f.factor = \frac{{}^9Be_{reactive} + {}^9Be_{diss}}{2.5}$

- eq 1' results in f.factors > 1
- eq 3 always results in the largest f.factor for a given study area
- methods don't agree

results, part 2. mean $^{10}\text{Be}/^9\text{Be}$ denudation rates

Table 4.

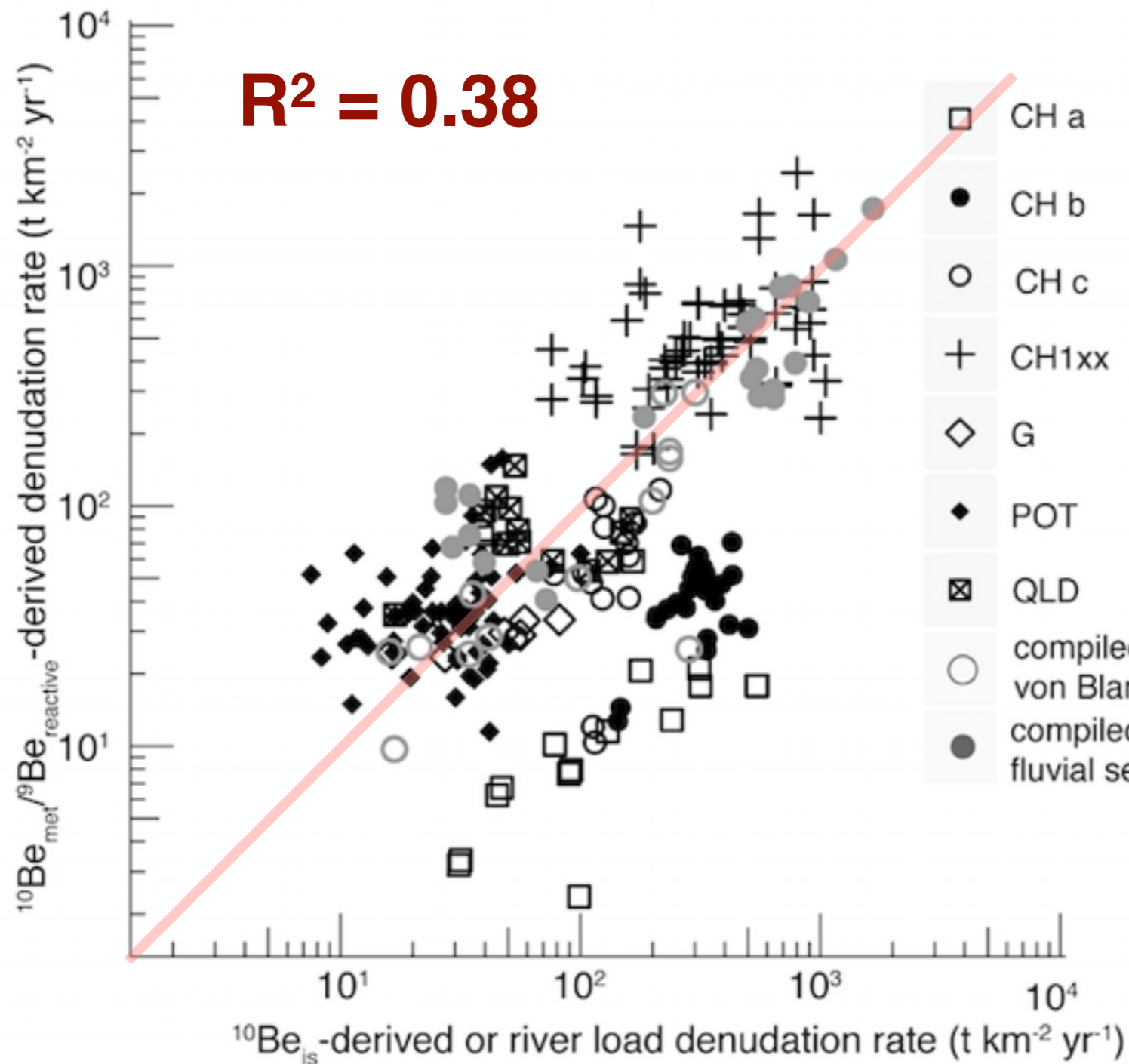
Mean denudation rates calculated from $^{10}\text{Be}_{\text{is}}$ and $^{10}\text{Be}_{\text{met}}/^9\text{Be}_{\text{reactive}}$ mass balance model (eq. 1) with ^9Be parent concentrations either assumed to be 2.5 ppm or the mean $^9\text{Be}_{\text{min}} + ^9\text{Be}_{\text{reactive}}$ for each basin.

Study	mean $^{10}\text{Be}_{\text{is}}$ - derived denudation rate ^a		mean $^{10}\text{Be}_{\text{met}}/^9\text{Be}_{\text{reactive}}$ - derived denudation rate (total parent $^9\text{Be} =$ 2.5) ^b		percent difference from $^{10}\text{Be}_{\text{is}}$ -derived denudation rate	mean $^{10}\text{Be}_{\text{met}}/^9\text{Be}_{\text{reactive}}$ - derived denudation rate (total parent = $^9\text{Be}_{\text{min}} + ^9\text{Be}_{\text{reactive}}$) ^b		percent difference from $^{10}\text{Be}_{\text{is}}$ -derived denudation rate
	t km ⁻² yr ⁻¹		t km ⁻² yr ⁻¹			t km ⁻² yr ⁻¹		
POT	30 ±	16	40 ±	26	35	141 ±	89	370
QLD	74 ±	45	81 ±	28	10	476 ±	162	543
G	44 ±	22	30 ±	4	35	133 ±	18	202
CH1xx	403 ±	268	552 ±	396	37	2030 ±	1450	404
CHa	160 ±	142	14 ±	14	-91	24 ±	14	-85
CHb	311 ±	88	42 ±	15	-86	259 ±	91	-17
CHc	128 ±	39	61 ±	33	-52	113 ±	61	-12
all samples	202 ±	226	205 ±	226	1	768 ±	1190	278

^a calculated with the CRONUS erosion rate calculator (Balco et al., 2008) in previous studies (Troodick, 2011; Portenga and Bierman, 2011; Nichols et al., 2014; Nielson, 2016)

^b total parent assumption applied to f.factor calculation and $^9\text{Be}_{\text{parent}}$; mean $^{10}\text{Be}_{\text{met}}$ deposition rate is used for each study area

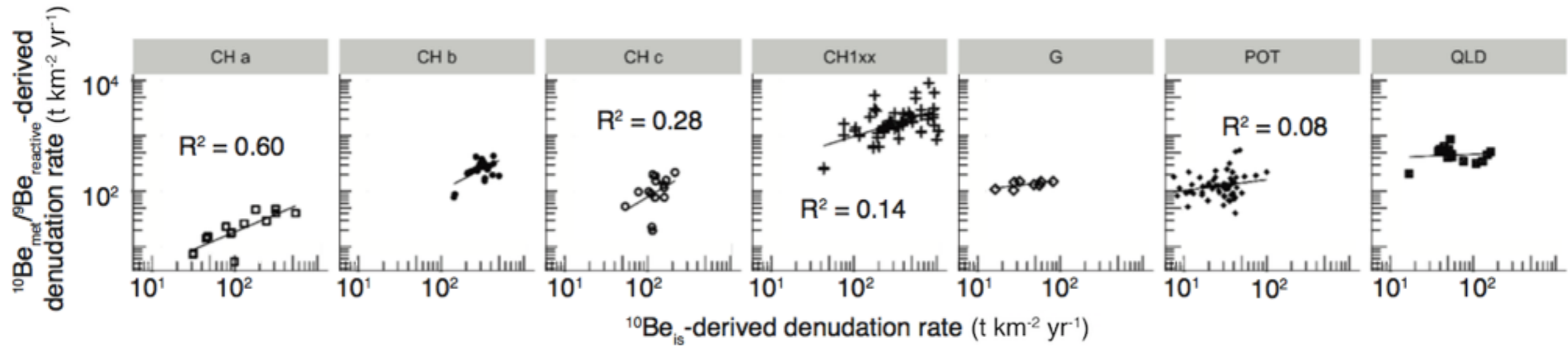
results, part 2. meteoric $^{10}\text{Be}/^9\text{Be}$ denudation rates significantly correlated to *in situ* denudation rates



- CH a
- CH b
- CH c
- + CH1xx
- ◇ G
- ◆ POT
- ⊠ QLD
- compiled from $(^{10}\text{Be}_{\text{met}}/^9\text{Be})_{\text{diss}}$ von Blanckenburg et al. (2012)
- compiled from $(^{10}\text{Be}_{\text{met}}/^9\text{Be})_{\text{reactive}}$ in suspended fluvial sed., von Blanckenburg et al. (2012)

- In agreement with von Blanckenburg et al. (2012) findings (grey)
- correlation not effected by assumptions about f.factor or parent ^9Be

results, part 2. meteoric $^{10}\text{Be}/^9\text{Be}$ denudation rates not significantly correlated to *in situ* denudation rates in many study areas



- no statistically significant correlation in 3 of 7 study areas
- R^2 is almost always < 0.30

discussion, part 2. how assumption influence $^{10}\text{Be}/^9\text{Be}$ denudation rates

$$D = \frac{F_{met}^{10\text{Be}}}{[^9\text{Be}]_{parent} * f.factor * \left(\frac{^{10}\text{Be}_{met}}{^9\text{Be}_{reactive}} \right)}$$

eq. 2

$$f.factor = \frac{^9\text{Be}_{reactive}}{^9\text{Be}_{reactive} + ^9\text{Be}_{min}}$$

$$[^9\text{Be}]_{parent} = ^9\text{Be}_{min} + ^9\text{Be}_{reactive}$$

- assumes negligible ^9Be in dissolved phase
- underestimates dissolved ^9Be
- **underestimates parent ^9Be**

eq. 3

$$f.factor = \frac{^9\text{Be}_{reactive} + ^9\text{Be}_{diss}}{2.5}$$

$$[^9\text{Be}]_{parent} = 2.5 \text{ ppm} = ^9\text{Be}_{reac} + ^9\text{Be}_{min} + ^9\text{Be}_{diss}$$

- assumes all “missing” ^9Be is from ^9Be in the dissolved phase instead of ^9Be in fine grained minerals
- overestimates dissolved ^9Be ;
overestimates f.factor

eq. 2 more likely to overestimate denudation rates

discussion, part 2. eq 2. does not consistently overestimate denudation rates

Table 4.

Mean denudation rates calculated from $^{10}\text{Be}_{\text{is}}$ and $^{10}\text{Be}_{\text{met}}/^{9}\text{Be}_{\text{reactive}}$ mass balance model (eq. 1) with ^9Be parent concentrations either assumed to be 2.5 ppm or the mean $^9\text{Be}_{\text{min}} + ^9\text{Be}_{\text{reactive}}$ for each basin.

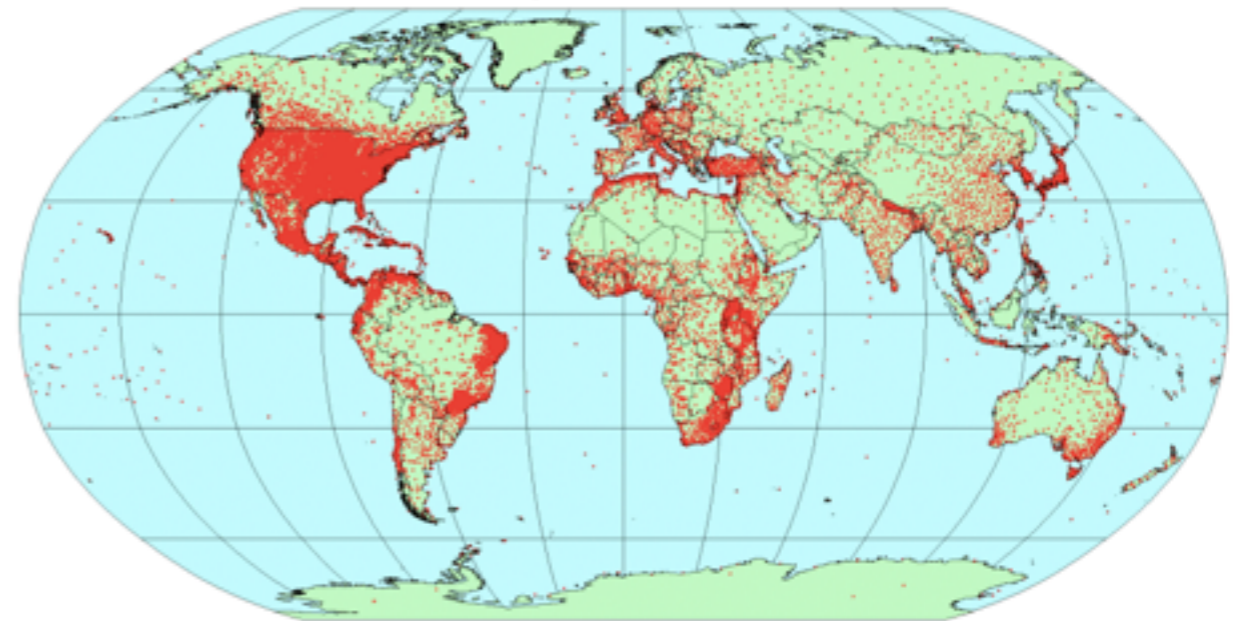
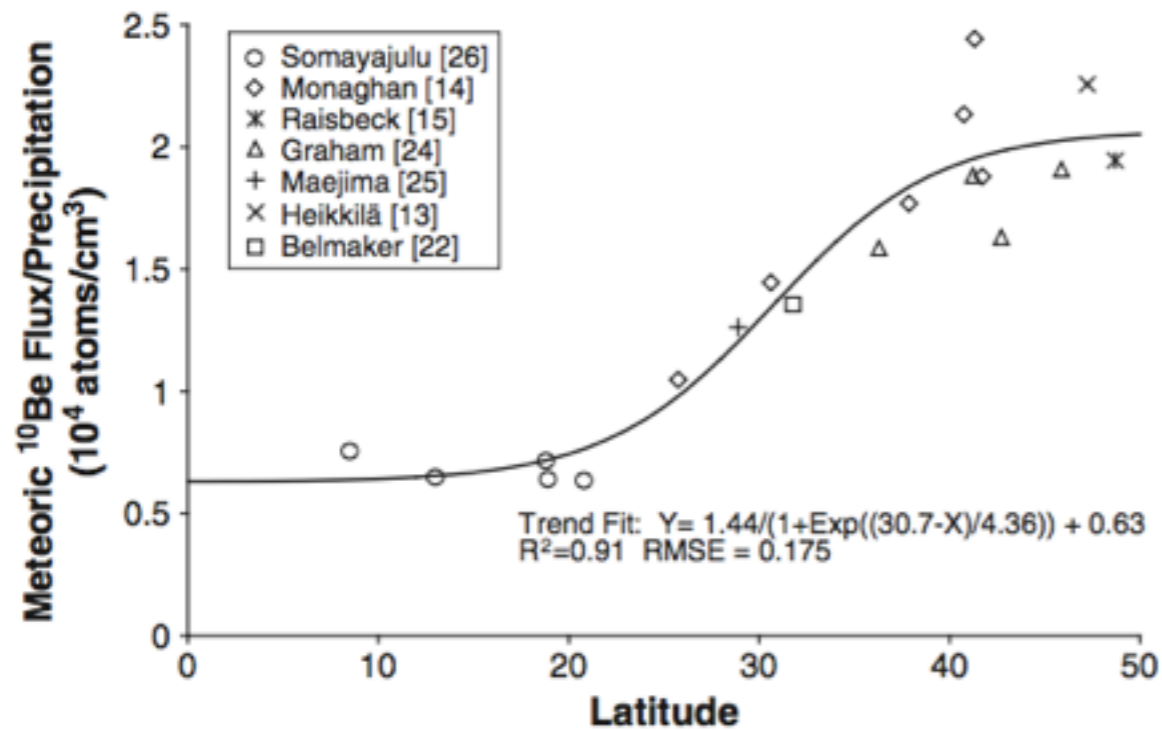
Study	mean $^{10}\text{Be}_{\text{is}}$ - derived denudation rate ^a		mean $^{10}\text{Be}_{\text{met}}/^{9}\text{Be}_{\text{reactive}}$ - derived denudation rate (total parent $^9\text{Be} =$ 2.5) ^b		percent difference from $^{10}\text{Be}_{\text{is}}$ -derived denudation rate	mean $^{10}\text{Be}_{\text{met}}/^{9}\text{Be}_{\text{reactive}}$ - derived denudation rate (total parent = $^9\text{Be}_{\text{min}} + ^9\text{Be}_{\text{reactive}}$) ^b		percent difference from $^{10}\text{Be}_{\text{is}}$ -derived denudation rate
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^b total parent assumption applied to f.factor calculation and $^9\text{Be}_{\text{parent}}$; mean $^{10}\text{Be}_{\text{met}}$ deposition rate is used for each study area


discussion, part 2. uncertainties in meteoric ^{10}Be delivery rates

Regional underestimate of meteoric ^{10}Be deposition rates in SW China study areas?



conclusions, part 2.

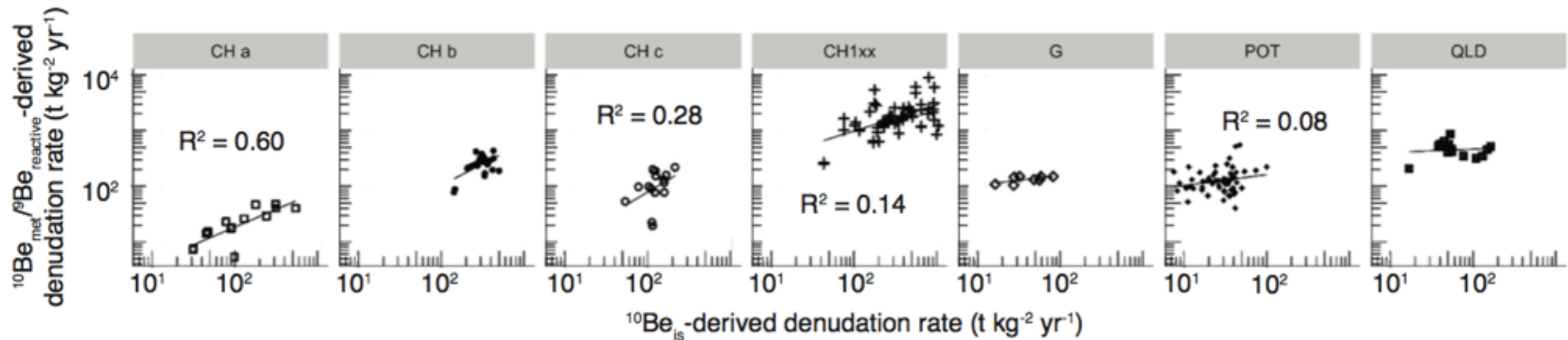
- Meteoric $^{10}\text{Be}/^9\text{Be}$ denudation rates agree with known in situ-based denudation rates across all samples
- uncertainties in parent ^9Be , f.factor, and meteoric ^{10}Be delivery rates, in addition to biogeochemical influences on meteoric $^{10}\text{Be}/^9\text{Be}$, add noise to the denudation rate proxy

The background of the slide is a classic marbled paper pattern. It features a complex, organic design with swirling, vein-like patterns in shades of light beige, cream, and off-white, interspersed with streaks and patches of muted grey and brown. The overall effect is a rich, textured, and somewhat abstract visual.

Thank you!

Questions?

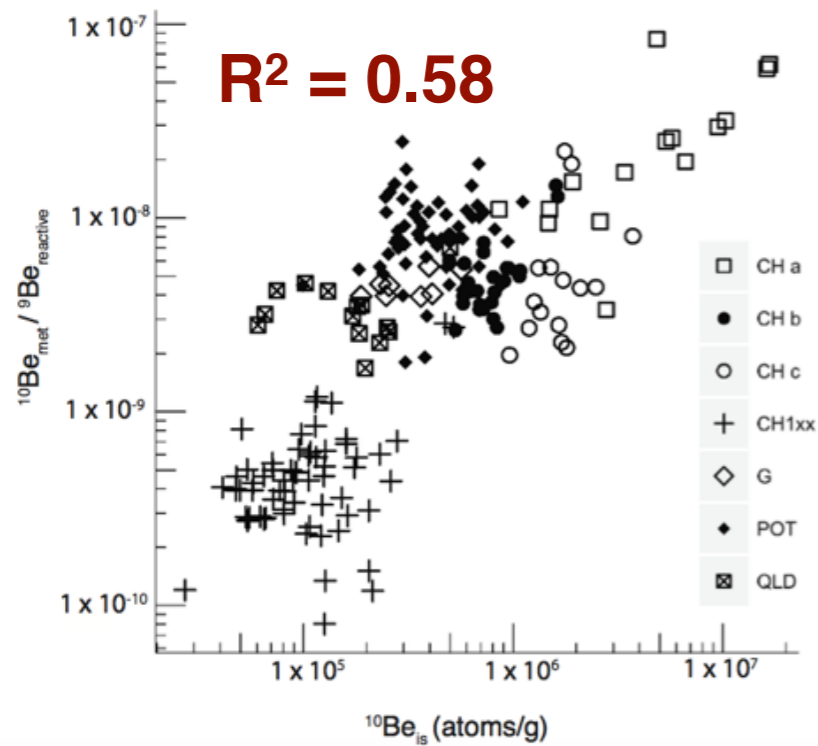
discussion, part 2. uncertainties in meteoric ^{10}Be delivery rates add noise to correlation between denudation rates



- heterogeneities in ^9Be parent concentrations and meteoric ^{10}Be delivery rates within study areas not quantified in mass balance model
- meteoric $^{10}\text{Be}/^9\text{Be}$ is influenced by leaching and remobilization

future work

meteoric $^{10}\text{Be}/^9\text{Be}$ ratios influenced by biogeochemical processes (stronger influence on regional scale) and spatial heterogeneity in Be inputs (stronger influence across all data)



- correlation between meteoric ^{10}Be and reactive ^9Be
 - meteoric ^{10}Be delivery rates depend on precipitation rate and latitude
 - reactive ^9Be controlled by parent ^9Be concentrations and weathering rates
- no correlation between meteoric ^{10}Be to ^{10}Be delivery rates

